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# MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

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VOLUME II ARIZONA VERIFICATION STUDIES, FY 79 GEOTECHNICAL DATA BUTLER CDP, ARIZONA

PREPARED FOR SPACE AND MISSILE SYSTEMS ORGANIZATION (SAMSO) NORTON AIR FORCE BASE. CALIFORNIA



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VOLUME II, ARIZONA
VERIFICATION STUDIES, FY 79
GEOTECHNICAL DATA
BUTLER CDP, ARIZONA

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### Prepared for:

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15 November 1979

#### VOLUME II GEOTECHNICAL DATA, BUTLER CDP

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SECTION 1.0
GEOLOGIC STATION DATA

Column Heading

USCS

#### EXPLANATIONS OF GEOLOGIC STATION DATA

Geologic stations were established at selected locations throughout the CDP at which detailed descriptions of surficial basin-fill deposits or rock were recorded. Locations of all geologic stations are shown in Drawing 1, Activity Location Map. All data taken on surficial basin-fill units at these stations are listed in Table 1-1 and an explanation of the column headings in the table is given below. At stations where rock descriptions were made, only geologic unit designations are listed. A general explanation of all geologic unit symbols used in Verification Studies is included at the end of this section.

Table 1-1	Explanation
Station Number	Geologic stations are numbered sequentially. Where more than one geologic field team worked in a CDP, stations made by each team are differentiated with a letter (A, B, or C) following the station number.
Geologic Unit	Generic geologic unit only, i.e. the grain-size designation (f, s, g, c) is omitted from surficial basin-fill units. The letter B in the unit designation indicates a buried deposit not exposed at the surface.
MPS MM	Average maximum particle size in millimeters.
Grain Size (%B, %C, %G, %S, %F)	Estimated particle size distribution using the Unified Soil Classification System. Percentages of boulders (%B) and cobbles (%C) are based on the entire deposit, whereas percentages of gravel (%G), sand (%S) and fines (%F) are taken only on the fraction composed of particles less than 3 inches (76 mm) in diameter.

THORY HATIONAL, INC.

ification System.

Soil class according to the Unified Soil Class-

Munsell Color Soil color based on Munsell Soil Color Chart.

Source Rock Rock types of coarse clasts listed in order of Types(s) abundance.

\* Physical Properties

Data listed in columns 6 through 15 address specific soil properties. These are listed below in parentheses following the column heading number and are also listed at the bottom of Table 1-1. Data are coded with each numerical entry referring to a specific soil condition as listed below.

- 6 (Grain Shape) 1) Angular, 2) Subangular, 3) Subrounded,
   4) Rounded, 5) Well rounded
- 7 (Moisture 1) Dry, 2) Moist, 3) Wet Content)
- 8 (Plasticity 1) None, 2) Low, 3) Medium, 4) High of Fines)
- 9 (Consistency) Coarse grained: 1) Very Loose, 2) Loose, 3) Medium Dense, 4) Dense, 5) Very Dense,

Fine grained: 1)Soft, 2) Firm, 3) Stiff,
4) Hard

- 10 (Structure)
  1) Stratified Tabular, 2) Stratified Other (lensed, cross bedded, discontinuous beds),
  3) Nonstratified
- 11 (Cementation 1) None, 2) Weak, 3) Moderate, 4) Strong Induration)
- 12 (Depth to Depth to layer (in centimeters) exhibiting Cemented cementation induration described in Column 11 Layers)
- 13 (Weathering 1) Fresh, 2) Slight, 3) Moderate, 4) Very of clasts)
- 14 (Soil 1) None (A-C profile), 2) Poor (incipient Profile B-horizon), 3) Well (prominant B-horizon) Development)
- 15 (Caliche 1) Stage I, 2) Stage II, 3) Stage III, Development) 4) Stage IV, 5) None

Dr	a	i	n	ad	e
	•	•			•

DP (M) WD (M)	Average depth of drainages (in meters) Average width of drainages (in meters)
Slope (%)	Average slope of ground surface (in percent grade)
Sample	Number of samples taken

#### GENERALIZED GEOLOGIC UNITS

#### Explanation

#### Surficial Basin-fill Units

- Al Younger Fluvial Deposits Major modern stream channel and flood-plain deposits.
- A2 Older Fluvial Deposits Older incised stream channel and flood-plain deposits in elevated terraces bordering major modern drainages.
- A3 Eolian Deposits Wind-blown deposits of sand occurring as either thin sheets (A3s) or dunes (A3d).
- A4 Playa and Lacustrine Deposits Deposits occurring in modern, active playas (A4) or in either inactive playas or older lake beds and abandoned shorelines associated with extinct lakes (A4o).
- As Alluvial Fan Deposits Alluvial deposits consisting of debris flow and water-laid alluvium near mountain fronts, grading into predominantly water-laid alluvium deposited in shifting distributary channels near the basin center. Younger (A5y), intermediate (A5i), and older (A5o) alluvial fans are differentiated by surface soil development, terrain conditions, and present depositional/erosional environment.

Grain sizes of these deposits (except A3 deposits, which are exclusively sandy) are indicated by a single letter (f, s, g, of c) following the geologic unit symbol. These letters indicate the predominant grain size and range of soil types according to the Unified Soil Classification System:

- f fine-grained (ML, CL, MH, CH)
- s sands (SP, SW, SM, SC)
- g gravels (GP, GW, GM, GC)
- c coarse grained with greater than 30 percent boulders and cobbles (generally GP, GW, GM, GC)

#### ROCK UNITS

- I Igneous (undifferentiated). Rocks formed by solidification of a molten or partially molten mass.
  - Il Intrusive Plutonic rocks formed by solidification of molten material beneath the surface (e.g., granite, granodiorite, diorite, gabbro).
  - I2 Extrusive (intermediate and acidic) Volcanic rocks of intermediate and acidic compositon formed by solidification of molten material at or near the surface, (e.g., rhyolite, latite, dacite, andesite).
  - I3 Extrusive (basic) Volcanic rocks of basic composition, generally formed by solidification of molten materials at or near the surface (e.g., basalt).
  - I4 Extrusive (pyroclistic) Rocks formed by accumulation of volcanic ejecta (e.g., ash, tuff, welded tuff, agglomerate).
- S Sedimentary (undifferentiated) Rocks formed by accumulation of clastic solids, organic solids and/or chemically precipitated minerals.
  - Sl Arenaceous and/or Siliceous Rocks Composed of sand size particles (e.g., sandstone, orthoguartzite) or of cryptocrystalline silica (e.g., opal, chert).
  - S2 Carbonate Rocks Composed predominantly of calcium carbonate detritus or chemical precipitates (e.g., limestone, dolomite, chalk).
  - S3 Argillaceous Rocks Composed of clay and silt-sized particles (e.g., siltstone, shale, claystone).
  - S4 Evaporite Rocks Precipitated from solution as a result of evaporation (e.g., halite, gypsum, anhydrite, sylvite).
  - S5 Coarse Clastic Rocks Composed of gravel sized or larger clasts (e.g., conglomerate, breccia).
- M Metamorphic (undifferentiated) Rocks formed through recrystallization in the solid state of preexisting rocks by heat and pressure (e.g., gneiss, schist, hornfels, metaquartzite).

	+ n 1			1 F R F A L N
STATION NUMNER	SEOL MPS GPAIN SIZE UNIT MR BR BC BG BS BF USES	MUNSELL SOURCE COLOR MOEK TANLESS	*PHYSICAL PROFESTICS 6 7 8 9 10 11 12 15 14 15	DENTALGE SEVEL
ALPGOIA ALPGOIC ALPGOIC ALPGOIC ALPGOIC	A57 070 00 07 20 060 020 SF A55 020 00 00 07 285 015 SV A51 140 08 02 20 060 027 C A51 058 15 065 C. SF A51 140 00 07 35 045 020 SF A1 140 00 07 25 055 020 SF	10-04F4/4 12 P 07-548/6 M [2 S] 05-048/6 M [2 S] 07-548/4 M [2 07-548/4 P 07-548/4 M	7 1 1 7 2 1 1 5 1 1 5 1 1 5 1 1 1 5 1 1 1 1 5 1	+0 000 00 0 1 1+0 000 00 1 1+0 003 01 7 4+0 01 01 0 3+0 005 01 1
ALPGOOD ALPGOOD ALPGOOD ALPGOOD ALPGOOD ALPGOOD	A2 175 00 01 76 075 005 51 A55 030 00 00 074 020 FH A51 190 00 07 25 770 005 5P-5H 451 100 00 07 25 770 006 020 6H A2 100 00 07 20 065 315 SH A35 007 01 07 20 050 020 6F A57 100 00 07 30 050 020 FH	10-01794/4 [1   2 M 51 07-51794/6 [2 M 07-51787/6 M 51 07-51787/6 M 51 07-51787/6 M 51 07-51787/4 M 12 52 07-51784/4 [2 M	5 1 1 5 2 1	5.0 C%C 07 0 5.0 250 C1 1 5.0 020 C2 0 -1 001 G7 1 -0 140 C2 1 1.0 005 G0 1
ALPGORA ALPGORA ALPGORA ALPGORA ALPGORA ALPGORA	ANT 000 00 01 UT 000 000 CF ANT 000 00 07 15 065 020 CF ANT 000 00 07 16 065 020 CF ANT 530 07 10 00 035 011 CM ANT 000 00 00 02 023 011 CM ANT 200 00 05 15 060 020 CM ANT 150 US 55 15 010 0F-GF	97-5985/6 M IC 97-5985/6 12 M 10-0098/- M H 97-5985/6 M 12 97-5985/6 M I2	2 1 2 3 3 2 027 1 1 5 2 2 1 3 7 1 7 028 1 1 5 2 1 2 3 1 2 028 1 1 5 2 1 2 3 1 2 3 1 5 2 2 1 1 1 3 3 3 2 028 3 2 2 1 1 1 2 2 1 1 1 2 2 1 1 1 1 2 2 1 1 1 1 2 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 3 3 2 2 2 2	-0 000 02 4 -2 001 00 1 -C 000 00 1 -0 000 00 1 -0 000 00 0 -7 001 00 1
ALPG11A ALPG11B ALPG12A ALPG12B ALPG13A ALPG13D ALPG14A	ASI 21C 07 10 54 C30 110 GP-GP ASI 130 05 55 035 010 GP-GP ASY 21C 00 05 40 C50 005 SP-SF ASI 150 07 05 55 030 015 GP-GP ASY 080 00 07 5C 045 C95 GP-GP AI 100 00 00 05 092 802 SF ASY 080 00 00 10 065 025 SF	H 10.0 YR4/4 H 10.0 YR4/4 H 07.5 YR5/6 H 12 10.0 YR4/4 I2 H 10.0 YR4/4 N	2 1 1 4 3 2 000 ? 3 2 1 1 1 2 7 2 050 ? 1 2 2 1 1 2 1 1 5 1 5 1 1 2 1 3 2 1 7 1 1 2 1 1 2 7 1 7 1 1 2 2 1 1 3 3 1 1 1 1 5 2 2 1 1 3 3 1 2 1 1	1.0 001 61 7 3.0 000 02 6 2 001 00 1 5.0 015 04 0 1 001 00 0 1 001 00 0 1 001 00 0
ALPSIAB ALPSISA ALPSISA ALPSISA ALPSISA ALPSITA ALPSITB	ASI 100 00 07 05 0A0 015 SM AP 673 00 07 35 050 015 SM ASI 090 00 C7 10 075 C15 SM A1 033 00 00 C7 C85 015 SM A51 200 00 00 70 52 010 GP-GM A2 060 00 00 70 020 010 GP-GM	07-5785/6 F I2 I1  F 52 I2  10-0786/4 H  07-5785/6  07-5784/6 I2 F  F 52 I2	7 2 1 3 2 2 808 2 2 2 4 2 1 4 3 3 827 3 1 3 2 1 1 3 3 2 806 2 2 1 3 2 1 2 3 1 7 1 7 5 3 2 856 2 3 1 4 1 1 4 3 3 818 2 2 3	5.5 CO1 OO 1 -3 OO1 O1 O 1.5 CO5 O 1
ALPGIBA ALPGIBB ALPGIBA ALPGIBB ALPGIBB ALPGIBB ALPGIB	A1 100 00 07 20 075 CDS SP-SM A2 083 00 00 60 00 20 027 6M A51 080 00 07 35 045 022 SC A7 060 00 07 35 045 022 SC A7 070 00 07 40 040 020 SM A30 025 00 00 00 080 50 15 SF A51 120 07 05 25 045 025 SL	10.0784/4 H 07.57P5/6 H 12 S2 10.0784/6 P	3 2 1 2 7 1 2 1 5 2 1 5 2 3 4 1 1 4 5 3 010 5 2 3 2 2 4 1 5 4 5 2 026 7 3 2 4 1 1 1 5 2 1 1 3 3 1 1 7 1 1 1 5 2 1 1 2 3 3 1 7 1 1 1 5 2 1 2 3 3 2 030 3 3 3 2	1.0 150 1 6.0 25. J 1.5 C3C 02 1 1.6 002 04 1 1.0 000 02 0 12.0 008 02 1
ALPG21H ALPG22A ALPG22H ALPG23A ALPG24A ALPG24A	AST 050 00 0T 15 060 C2* SF AST 100 00 05 55 020 010 GP-6F AST 125 0C 10 65 020 015 GF AST 110 00 07 40 040 020 SC AST 125 00 10 30 055 015 SF ASO 350 05 10 60 020 001 CP-6F 451	07-5485/6 M 12 H 17 K 17 I1 07-5489/6 H 07-5485/6 I2 M 52 H I1	2 1 1 2 2 2 C <sup>4</sup> <sup>4</sup> 2 1 7 1 1 1 2 2 1 1 2 2 1 1 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 4 7 2 2 000 2 1 2	3.0 020 01 C 1.0 004 01 1 6.0 300 C 3.0 003 C 12.6 500 0 6.0 000 0+ 0
ALPG258 ALPG258 ALPG264 ALPG274 ALPG278 ALPG288	Aby 120 00 05 40 030 075 5% Abs 023 00 00 CT PRO 020 5F Abs 140 00 C5 50 025 020 CC Abs 018 00 CC 00 005 115 5P Abs 200 01 05 50 025 020 GP Abs 034 00 90 07 065 025 5C Abs 036 00 00 07 065 025 5F	07-5794/4 F 12 07-5794/6 11 07-5796/6 11 07-5795/6 F 12 10-0794/6 11	2 1 2 3 3 1 2 1 1 5 2 1 1 1 5 3 2 1 1 5 3 2 1 1 1 5 3 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.0 001 02 1 .0 002 05 1 1.0 002 07 1 1.0 002 07 1 2.0 001 01 1
ALPG238 ALPG298 ALPG308 ALPG309 ALPG318 ALPG31P		07.5YR5/6 M 12	2 1 1 2 3 1 2 7 2 7 2 2 1 2 3 5 3 2 050 2 7 2 7 2 2 2 1 2 3 3 2 050 2 1 1 2 1 1 2 3 3 2 050 2 1 1 1 2 1 2 3 3 3 1 2 1 5 3 2 1 1 2 3 3 1 1 1 5	00 00 01 1 0 00 00 00 00 00 00 00 00 00
ALPG32A ALPG32B ALPG33A ALPG34A ALPG34B ALPG35A		07.5YR5/6 M I2 S2 11 07.5YR5/6 M I2 S2 11 M 07.5YR5/6 I2 M 10.0YR4/6 P	5 1 1 3 2 1 2 2 1 5 1 1 3 3 2 647 ? 1 1 2 1 1 4 3 2 630 5 3 2 3 1 1 3 3 2 642 2 1 2 2 1 2 3 2 2 642 2 1 2 2 1 2 3 2 2 643 3 2 2 2 1 2 3 3 2 646 3 2 2 2 1 1 3 3 1 2 2 1	-5 002 00 1 -1 001 0J 7 -1 007 0z 7 1-0 010 0c 1 20-0 010 0c 0 -0 100 0c 0
ALPG35A ALPG36A ALPG36B ALPG37A ALPG38A ALPG38B	ASI 180 0T 10 35 035 010 (A-GF ASC 280 0T 65 57 030 015 G-G-G- ASI 100 0T 65 70 020 010 (A-G-G- ASI 100 0T 65 70 020 010 (A-G-G- ASI 300 0T 10 35 036 015 (A-G-G-G-G-G-G-G-G-G-G-G-G-G-G-G-G-G-G-G	12 M S2 M 12 07-5YR4/6 M 12 M 12 M 11 10-0YR7/4 M	2 1 1 2 3 1 4 1 1 2 3 7 2 1 2 3 7 2 2 1 1 3 2 2 0 0 3 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 3 5 5 5 0 0 7 2 3 2 1 1 1 3 3 5 0 0 7 2 3 2 1 1 1 3 3 5 0 0 7 2 3 2 1 1 1 3 3 5 0 0 7 2 3 2 1 1 1 3 3 2 0 1 4 7 1 2 1 2 1 1 4 3 2 0 1 4 7 1 2 1 2	5-E 031
ALPG39A ALPG40A ALPG40A ALPG41A ALPG41B ALPG42A	A51 080 00 00 10 075 015 50 A51 180 00 12 7 0 015 015 07 A57 990 00 07 20 060 020 5P A51 180 07 10 55 075 020 6C A1 280 07 05 60 025 010 029-6P A1 350 07 10 55 080 03 5P A51 150 00 07 55 035 010 079-6P	07-5YR4/6 * 07-5YR5/6 12 11 H	2 1 2 3 3 2 040 2 3 1 5 1 1 4 2 2 030 2 2 2 2 2 1 1 3 3 3 2 044 2 1 1 3 1 1 3 3 2 024 2 3 2 2 1 1 2 3 1 7 1 5 2 1 1 2 3 1 7 1 1 3 2 1 3 2 2 3 1 7 1 1 4 3 2 1 3 2 2 3 1	-3 002 02 1 -5 050 01 0 -5 082 00 1 -5 082 01 0 -5 001 83 0 1-7 015 07 0
ALP642D ALP643A ALP643R ALP644B	ASI 176 DG 05 GC 020 G26 GC ASO 200 03 10 65 015 307 GK-GP ASI 300 07 10 60 020 020 GC ASI 25G 07 05 60 020 020 UP	12 13 12 14 12 11 M 52	2 1 2 3 7 1 2 3 1 2 1 1 4 3 3 000 2 3 2 3 1 2 3 3 2 042 2 3 2 2 1 1 3 2 2 020 2 3 7	3.0 030 02 0 3.0 030 02 C

GEOLOGIC STATION DATA
VERIFICATION SITE, BUTLER CDP, ARIZONA

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TABLE

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-PHYSICAL PROPERTIES : 6 - GRAIN SHAPE 7 - MOISTURE CONTENT # - PLASTICITY FIPES

y - COLSISTENCY 10 - STRUCTURE 11 - CEPENTATION-INDURATION SECTION 2.0
GROUND WATER DATA

#### EXPLANATIONS OF GROUND-WATER DATA

Existing ground-water data in Butler CDP were collected from all available sources. These data were updated where possible from measurements taken during Fugro field operations, and all data are shown in Table 2-1. Locations of water wells and boreholes in which water-level measurements were available are shown in Drawing 1. Well numbers listed in Column 1 (Table 2-1) refer to well locations in Drawing 1. Actual well numbers giving location according to the Bureau of Land Management Land Survey System are shown in Column 2.

Water levels generally refer to the static ground-water table in the unconfined basin-fill aquifer. Perched conditions or levels in artesian aquifers are noted where known.

•	WELL LOCATION Number*	ELEVATION	DEPTH OF WELL- FEET (METERS)	WATER LEVEL			
WELL No.		OF GROUND SURFACE- FEET (METERS) ABOVE M.S.L.		DEPTH BELOW GROUND SURFACE- FEET (METERS)	DATE MEASURED	ELEVATION - FEET (METERS) ABOVE M.S.L.	REFERENCES**/ REMARKS
Wl	(B-9-11) 30dcb	2380 (725)	65 (20)	36 (11)	1975	2344 (714)	3,4
W2	(B-8-12) 6aca	2010 (613)	-	735	-	1275	5
WЗ	(B-8-12) 23bcd	3300 (1006)	830 (253)	740 (226)	1975	2560 (730)	4,5
W4	(B-8-13) 4ddd	1790 (546)	1000 (305)	530 (162)	1974	1260 (384)	4,5
₩5	(B-8-13) 20ccc	1730 (527)	1350 (411)	-	-	-	2
W6	(B-8-14) 20dab	1522 (464)	545 (166)	244 (74)	1975	1278 (390)	4,5
W7	(B-8-14) 23daa	1620 (494)	730 (222)	340 (104)	1976	1280 (390)	4
W8	(B-8-14) 23dda	1618 (493)	1000 (305)	343 (104)	1977	(389)	4,5
W9	(B-8-14) 25cba	1645 (501)	1500 (457)	368 (112)	1975	(389)	4,5
W10	(B-7-9) 2ddc	1425 (434)	552 (168)	158 (48)	1978	(386)	4,5
Wll	(B-7-15) 9ddd	1365 (416)	145 (44)	95 (29)	1975	1270 (387)	4,5
W12 W13	(B-7-15) 10aac	1395 (425)	(207) <sup>'</sup>	-	-	-	2
W13	(B-7-15) 11ddd	1444 (440)	(305)	(52)	1975	(388)	4,5
W14 W15	(B-7-15) 12dad	1490 (454)	680 (207)	(66)	1975	(388)	4
MTO	(B-7-15) 21bab	1345 (410)	(62)	(23)	1967	1268 (386)	1,4
1							

\*Gila and Salt River Baseline and Meridian

#### \*\*References

- 1) Briggs (1969)
- 2) U.S. Bureau of Reclamation (1978)
- 3) U.S. Geological Survey (1975)
- 4) U.S. Geological Survey (1978)
- 5) Wilkins and Webb (1976)

GROUND WATER DATA
VERIFICATION SITE, BUTLER CDP, ARIZONA

NOTE: All wells tap unconfined alluvial aquifers except where noted. Where published data are lacking or inaccurate, ground surface elevations are taken from topographic maps.

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SECTION 3.0
SEISMIC REFRACTION DATA

#### EXPLANATIONS OF SEISMIC REFRACTION DATA

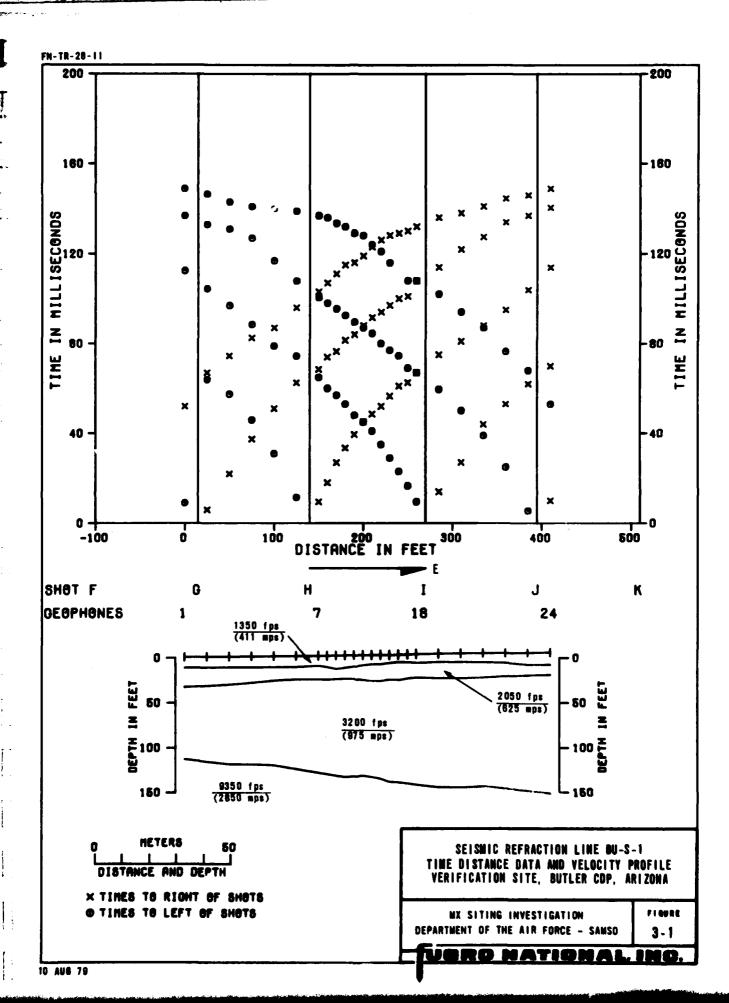
Each figure shows seismic wave travel times plotted versus surface distance between the energy source (shot) and the detector (geophone) for a single seismic line. Distances are measured along the line from geophone number 1 which is designated as zero distance. Distances to the right (on the paper) of geophone 1 are positive. The direction arrow gives the approximate direction of the geophone array from geophone 1 to geophone 24.

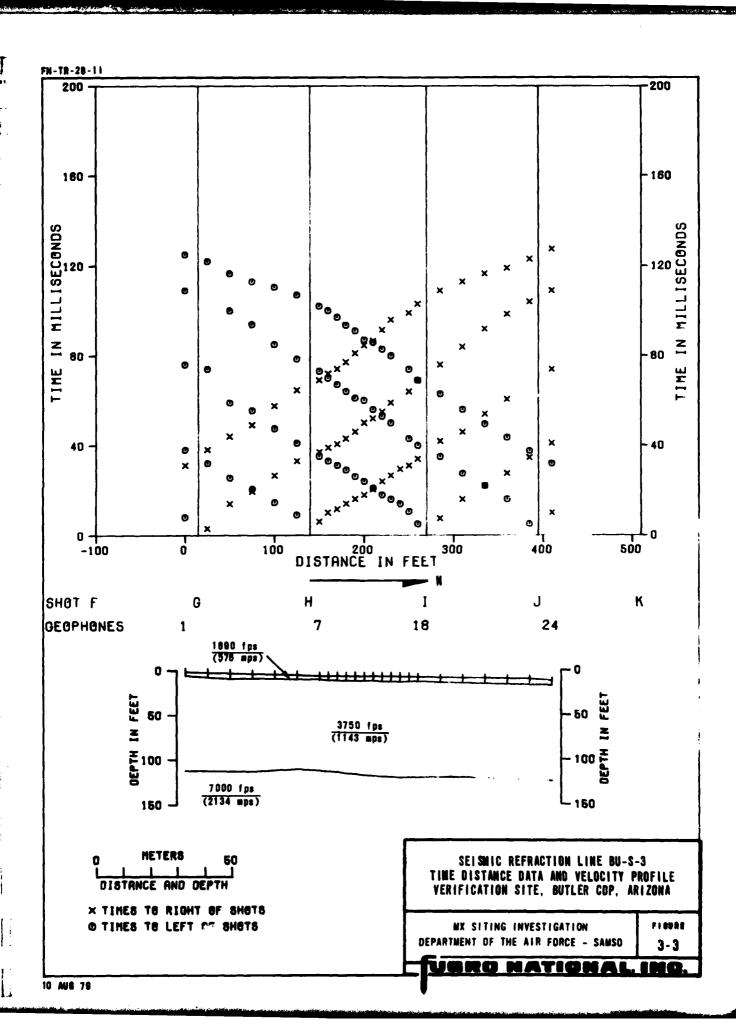
## Travel Time Versus Distance Graph (Upper Half of Figure)

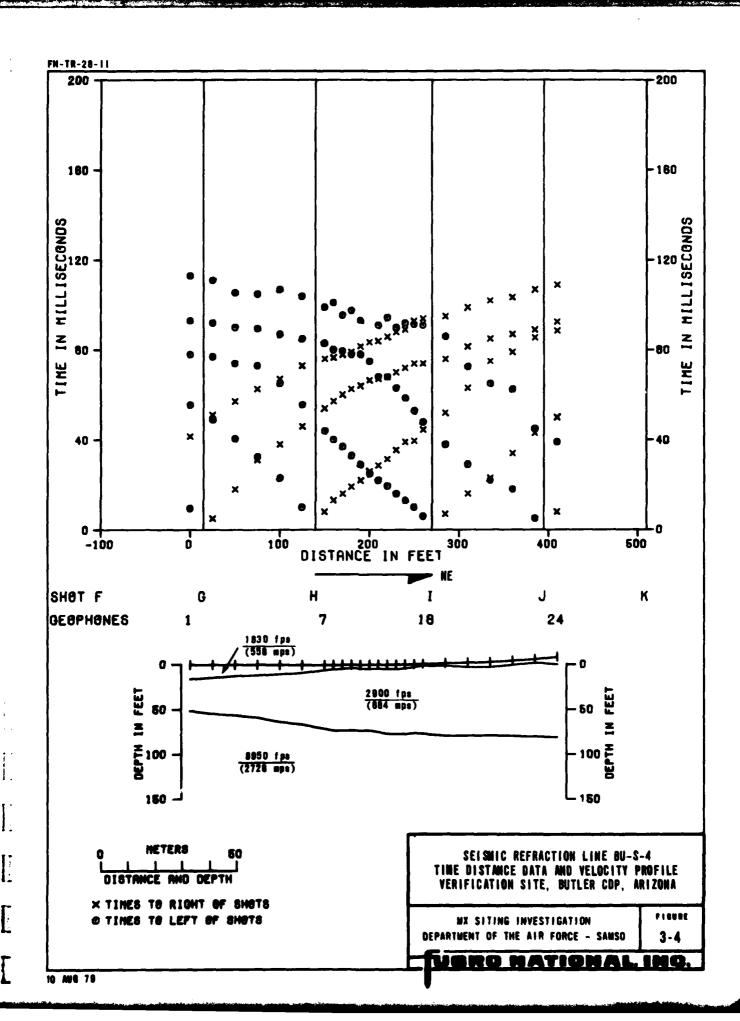
This is a travel time versus distance graph. The abscissa represents distance; the ordinate, time. The six vertical lines represent the locations of shots (designated as F, G, H, I, J, and K). The symbol, X, denotes travel times at geophones that were located to the right of a shot. The symbol, 0, denotes travel times that were located to the left of shots.

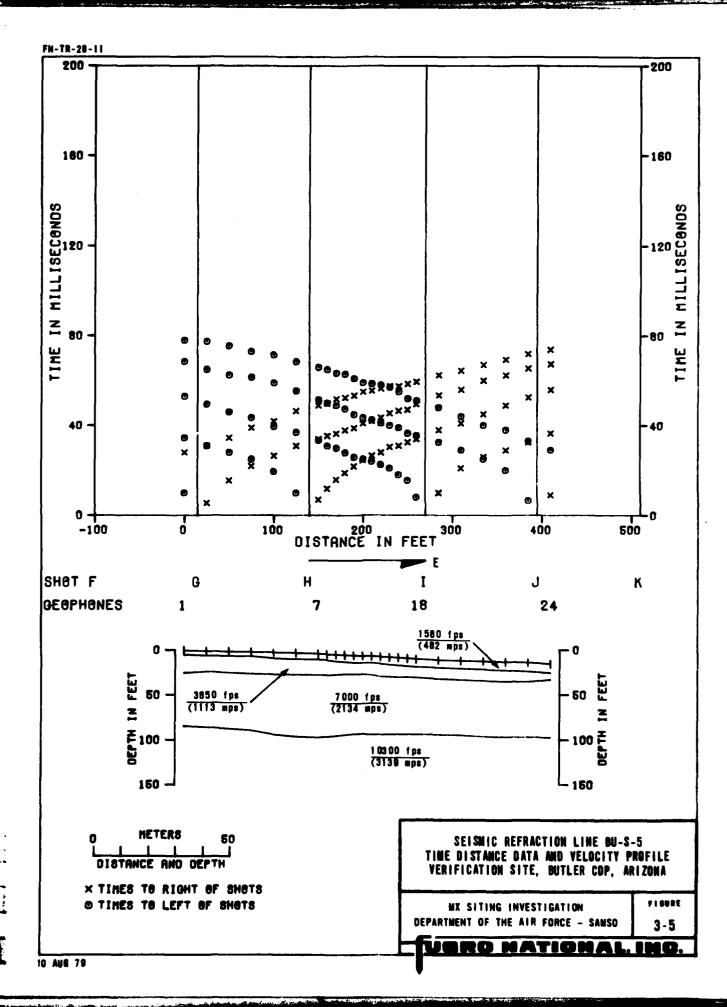
## Velocity Cross Section (Lower Half of Figure)

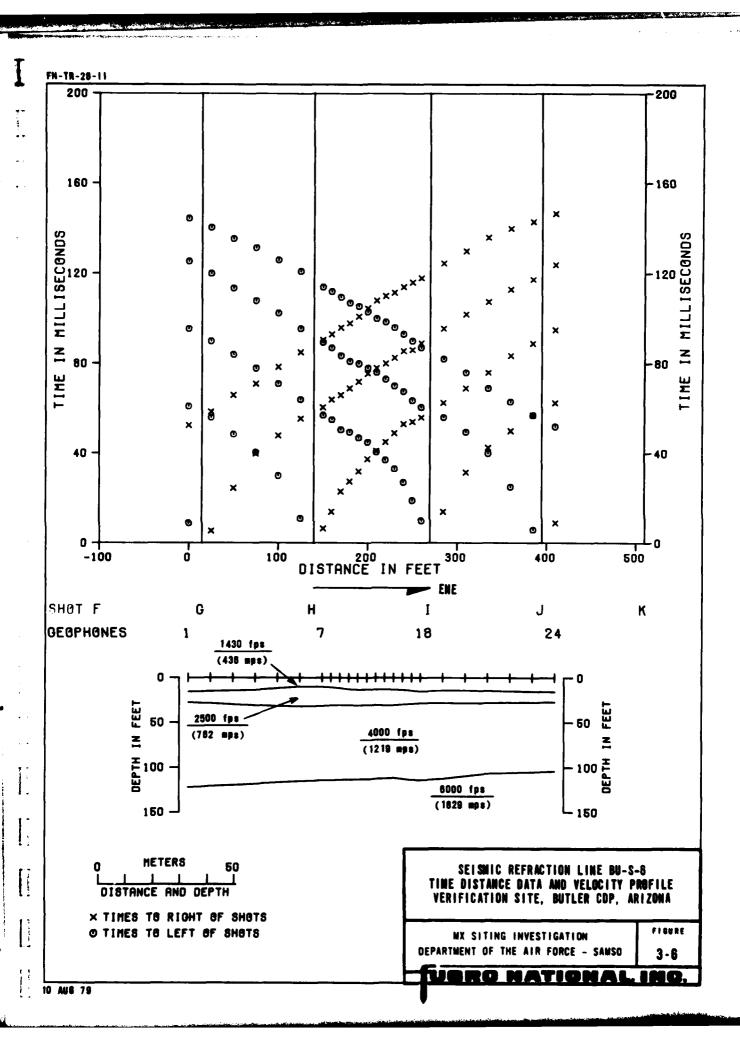
This is an interpreted velocity cross section beneath the seismic line. The top line represents the ground-surface profile. The short vertical lines crossing the top line mark the geophone positions. The depth scale is plotted relative to a point on the line which was arbitrarily chosen as "zero elevation" at the time the line was surveyed. The additional lines across the cross section represent the interpreted boundaries between layers of material with different compressional wave velocities. These boundaries are commonly called "refractors". The velocity interpreted to be representative of each layer is shown.

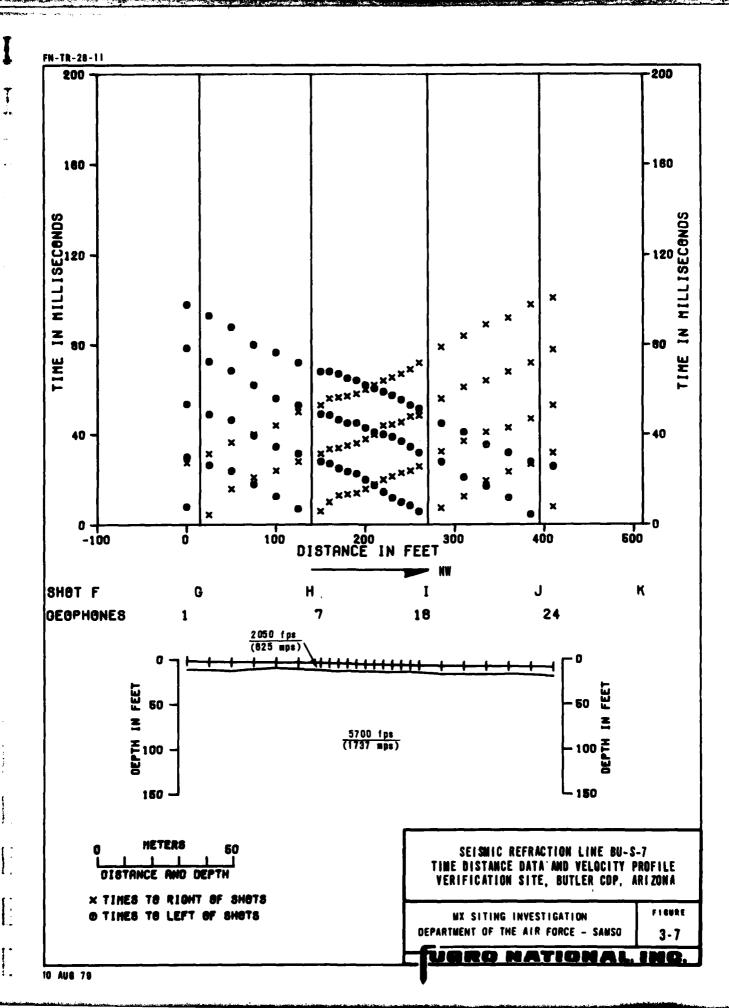


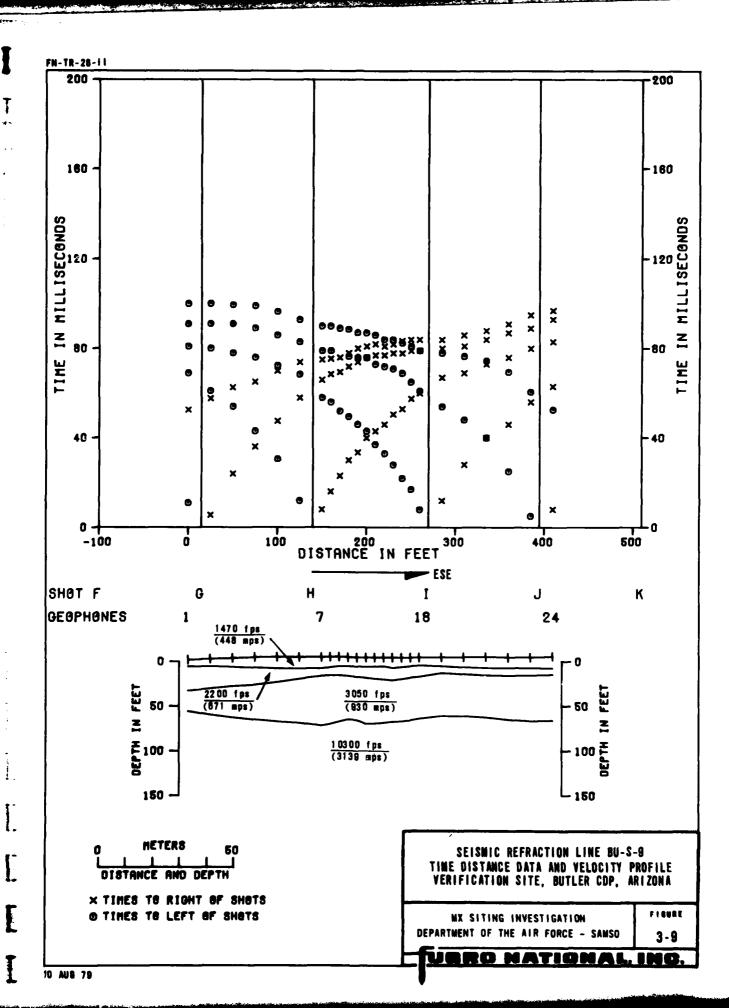


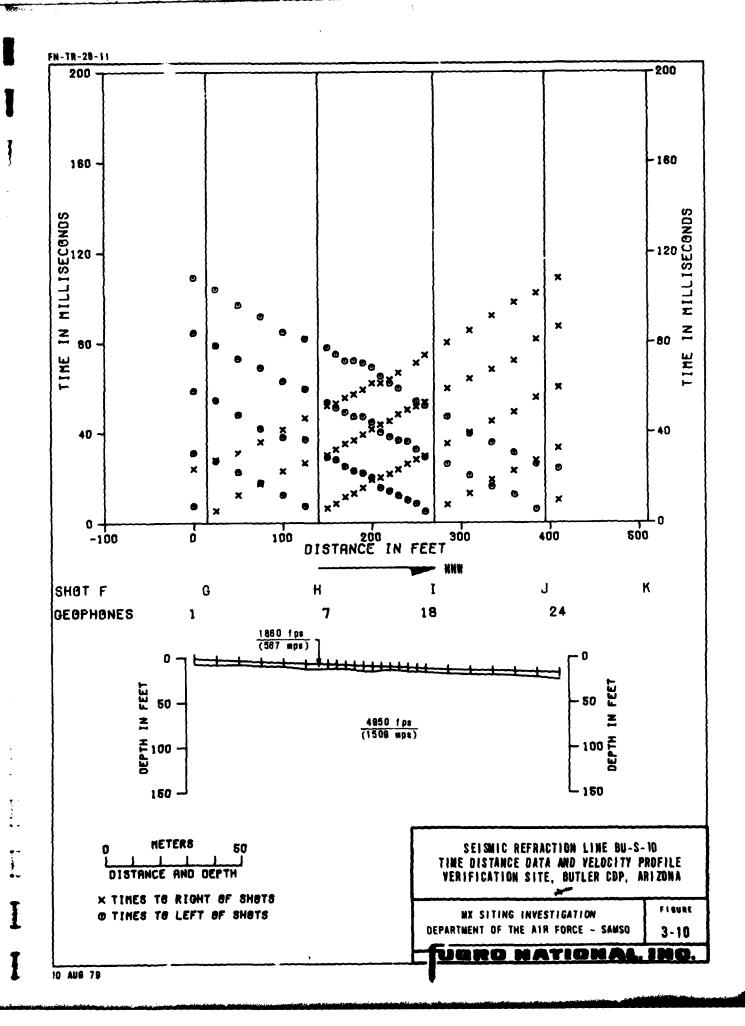


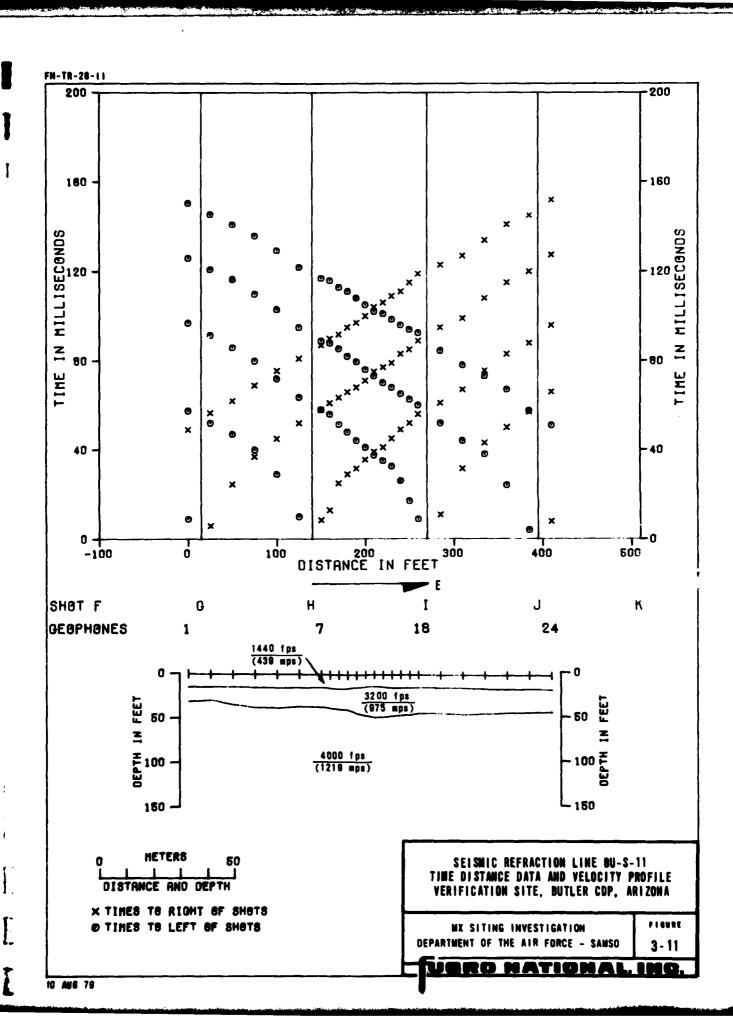


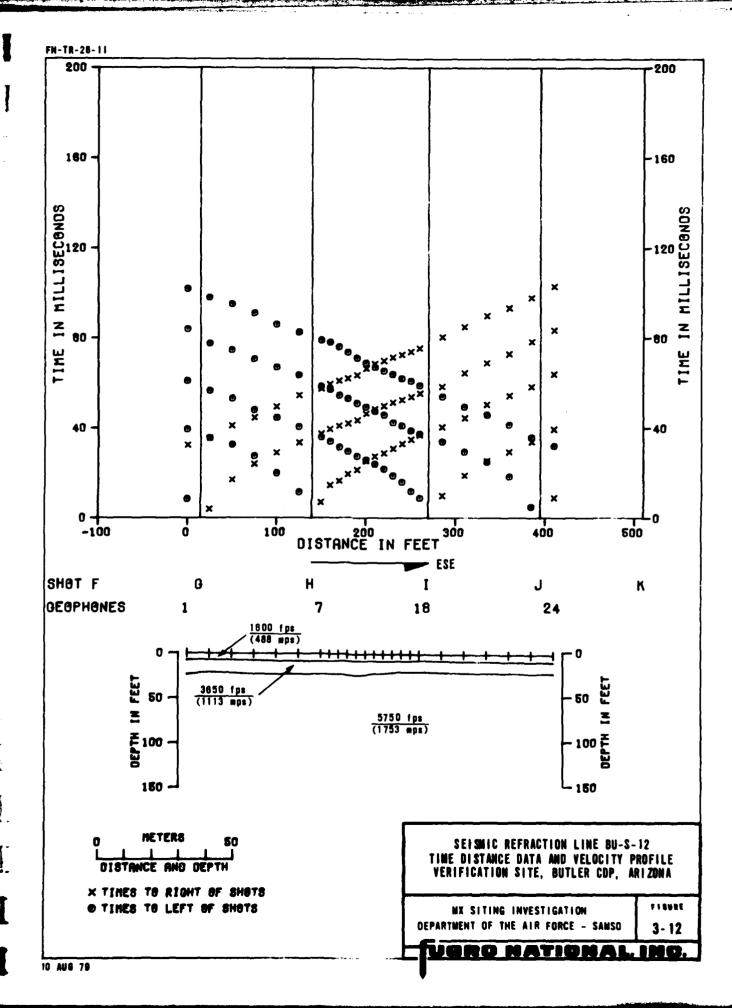


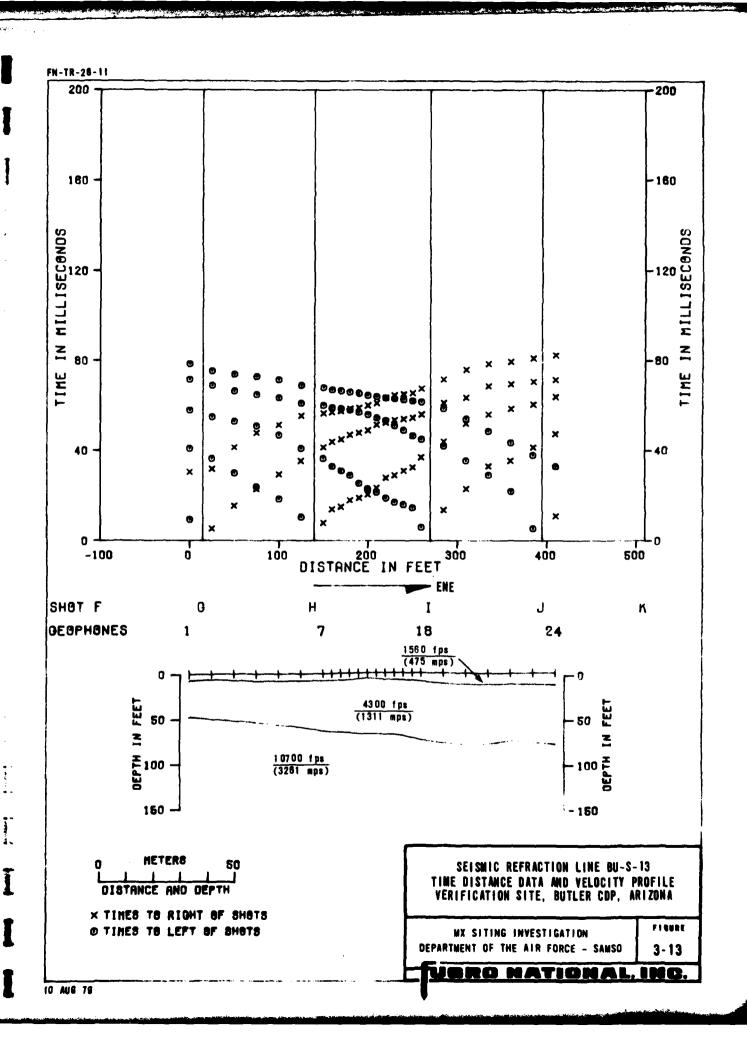


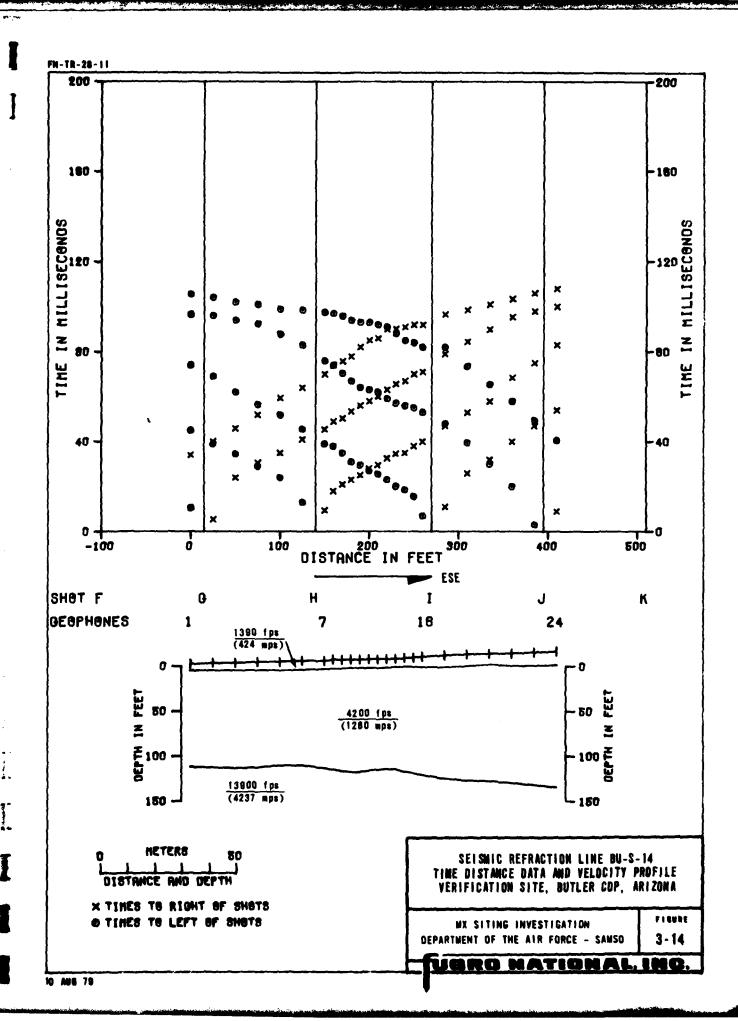


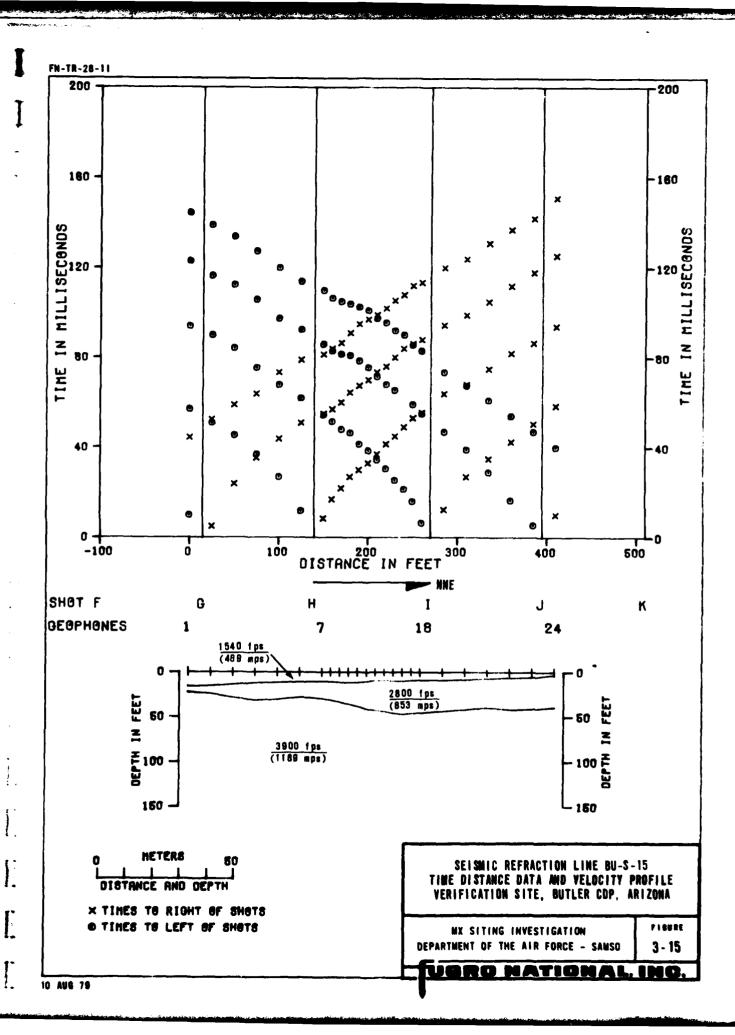


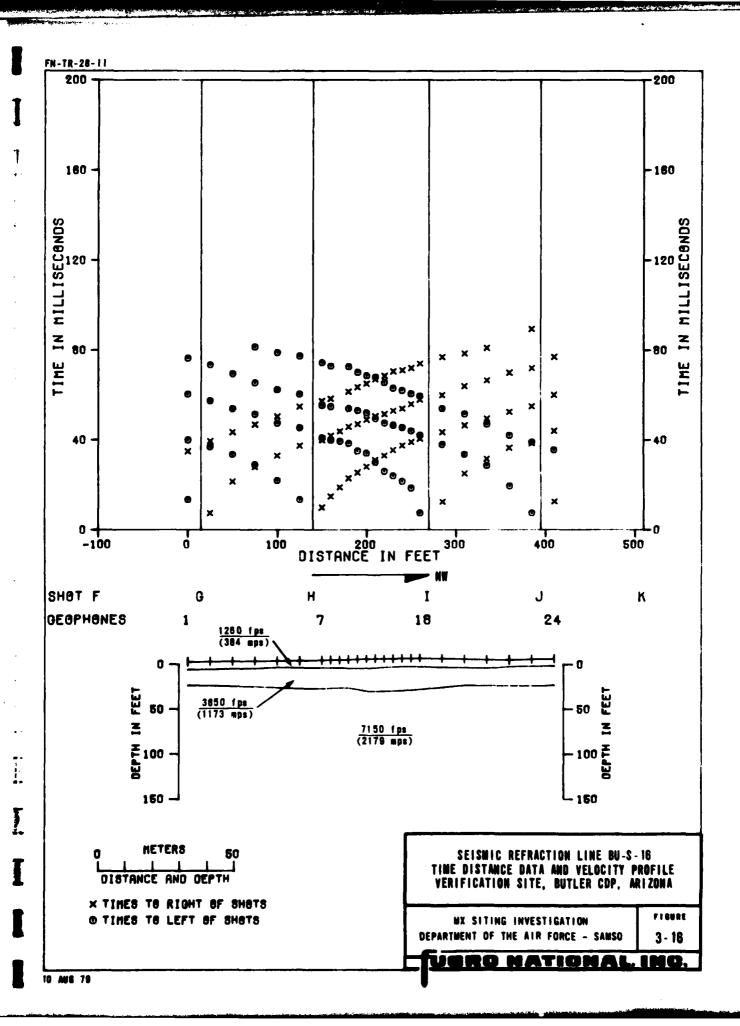












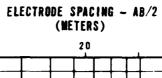
SECTION 4.0
ELECTRICAL RESISTIVITY DATA

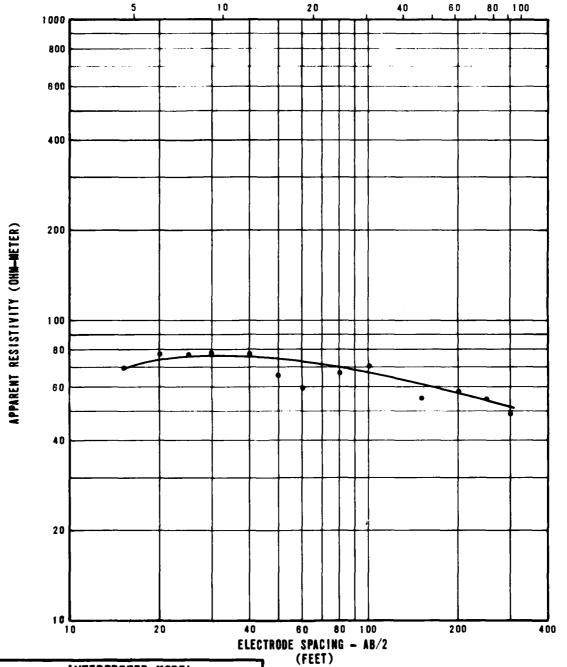
#### EXPLANATIONS OF ELECTRICAL RESISTIVITY DATA

Each figure in this section presents the data obtained from a resistivity sounding and a tabulated model of resistivity layers that would produce a curve similar to the observed curve.

The upper portion of the figures is a graph in which measured apparent resistivity values in ohm-meters are plotted versus one-half the distance between the current electrodes.

The interpreted model tabulated at the bottom of the page shows a combination of true resistivity layers and thicknesses obtained by matching theoretical curves to the field curve.

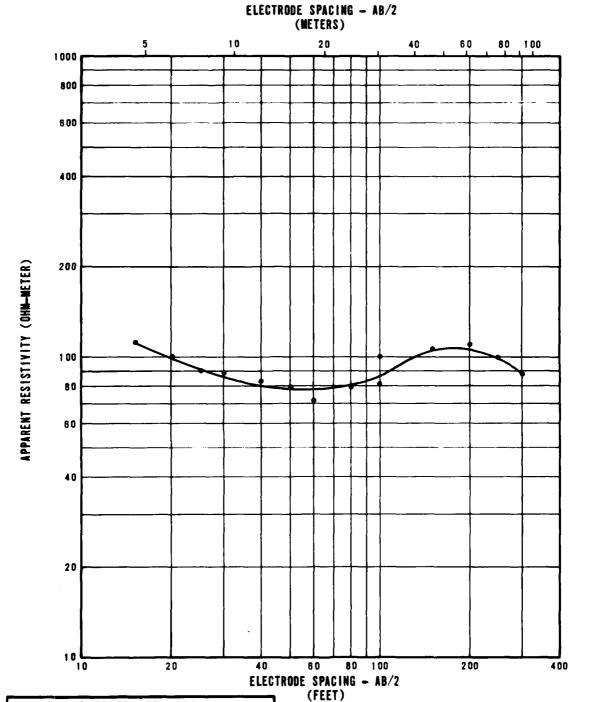




	INTERPRETED MODEL			
LAYE	LAYER DEPTH RESISTIVITY VALUES			
FEET	METERS	OHN-METER		
0	0	70		
15	5	85		
49	15	45		
		1		
	1	1		

RESISTIVITY SOUNDING BU-R-1 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE SAMSO FIGURE 4-1



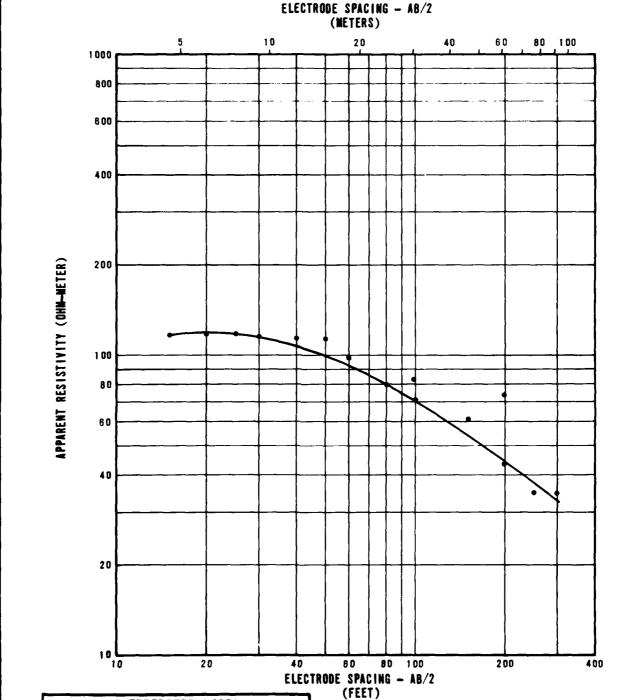
	INTERPRETED MODEL		
LAYE	LAYER DEPTH   RESISTIVITY VALU		
FEET	METERS	OHM-METER	
0	0	140	
5	2	80	
70	21	300	
92	28	150	
182	49	35	

RESISTIVITY SOUNDING BU-R-2 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

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DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE 4-2

UGRO NATIONAL INC.



	INTERPRETED MODEL		
LAYE	RDEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	120	
36	12	30	

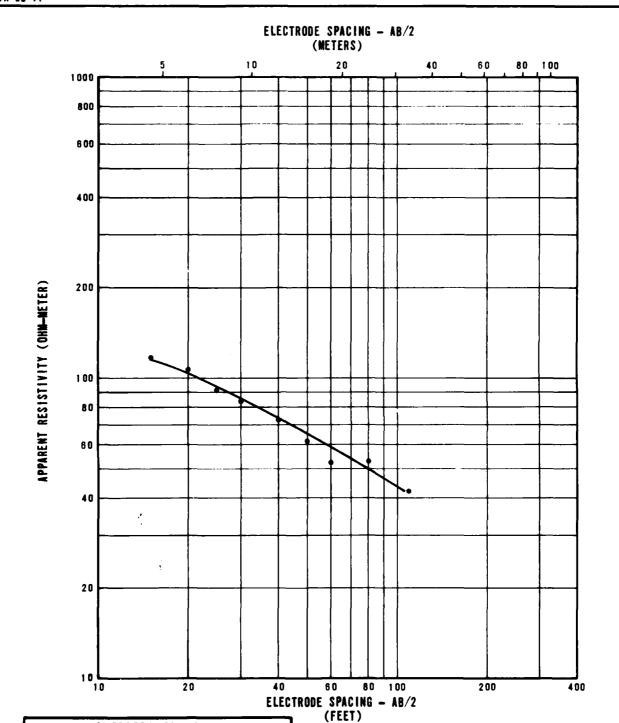
RESISTIVITY SOUNDING BU-R-3 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE SAMSO

f | GURE 4-3

**UGRO NATIONAL INC.** 



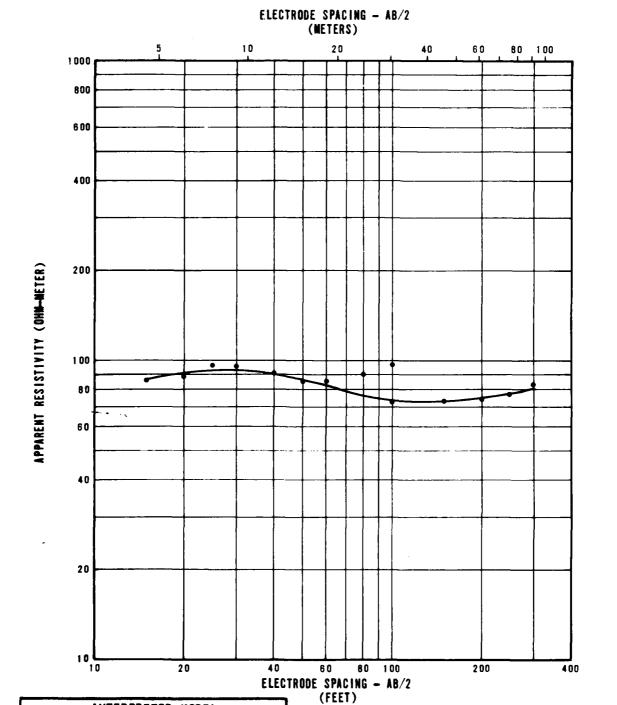
	INTERPRETED MODEL		
LAYE	LAYER DEPTH RESISTIVITY VALU		
FEET	METERS	OHM-METER	
0	0	130	
15	5	45	
79	24	20	
	1		

RESISTIVITY SOUNDING BU-R-5
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE, BUTLER CDP, ARIZONA

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DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE 4-4

UBRO NATIONAL INC.

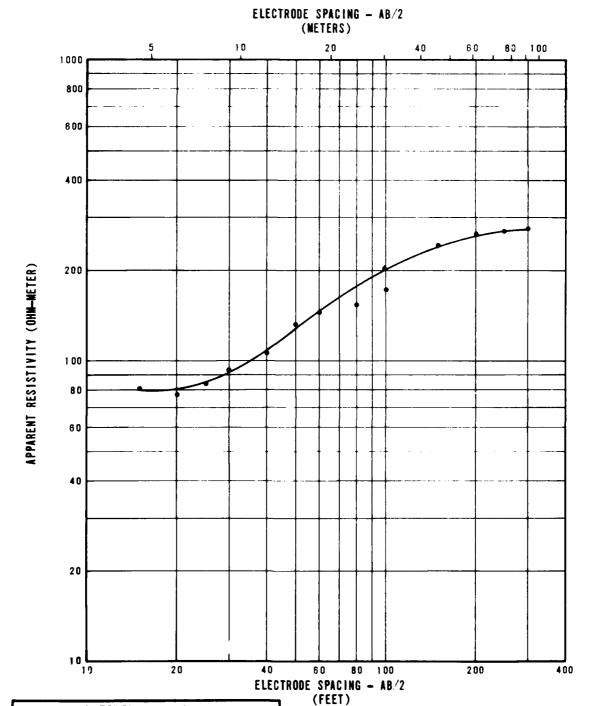


	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	100	
22	7	85	
115	35	100	
	Ī		

RESISTIVITY SOUNDING BU-R-6 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

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DEPARTMENT OF THE AIR FORCE SAMSO

FIGURE 4-5



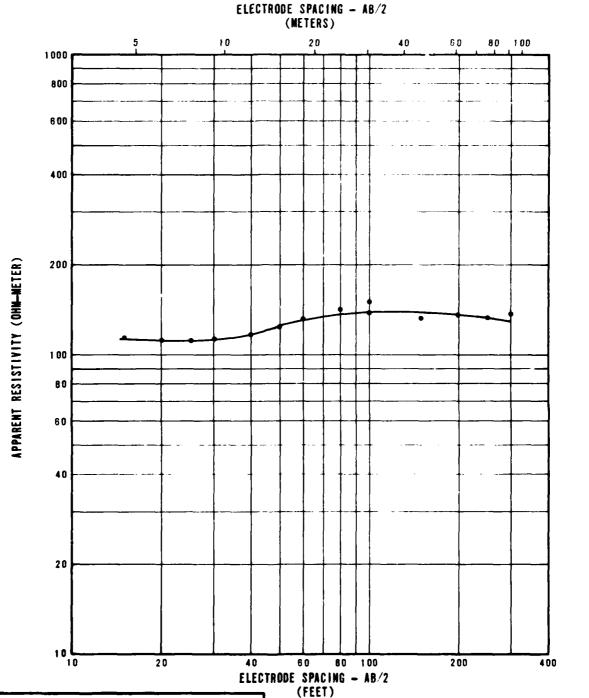
	INTERPRETED MODEL		
LAYES	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHN-METER	
0	0	75	
24	7	410	
158	48	190	
	Ī		
	1		

RESISTIVITY SOUNDING BU-R-7 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

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4-6

UGRO NATIONAL INC.



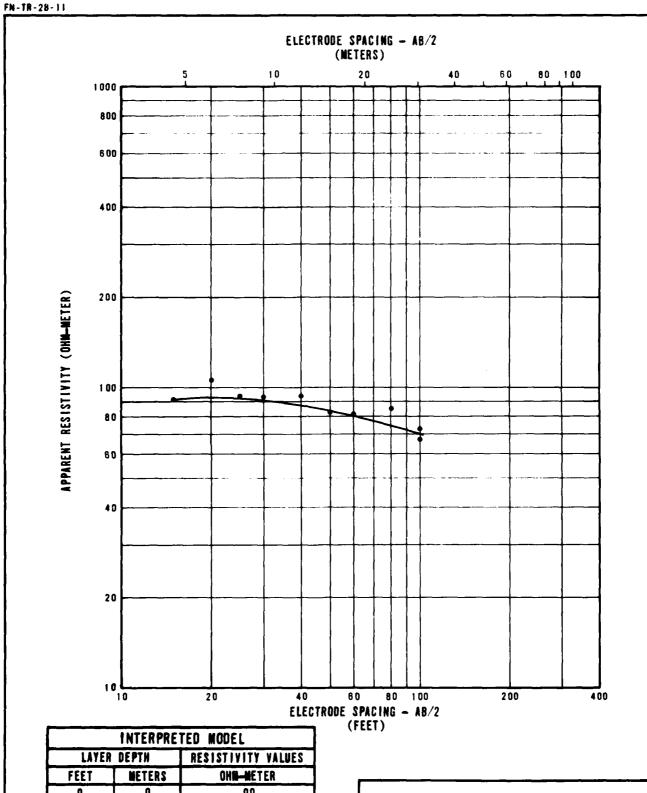
	INTERPRETED MODEL		
LAYE	RDEPTH	RESISTIVITY VALUES	
FEET	METERS	OHN-METER	
0	0	110	
37	11	210	
79	24	110	

RESISTIVITY SOUNDING BU-R-8
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE, BUTLER COP, ARIZONA

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DEPARTMENT OF THE AIR FORCE SAWSO

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UBRO NATIONAL INC.

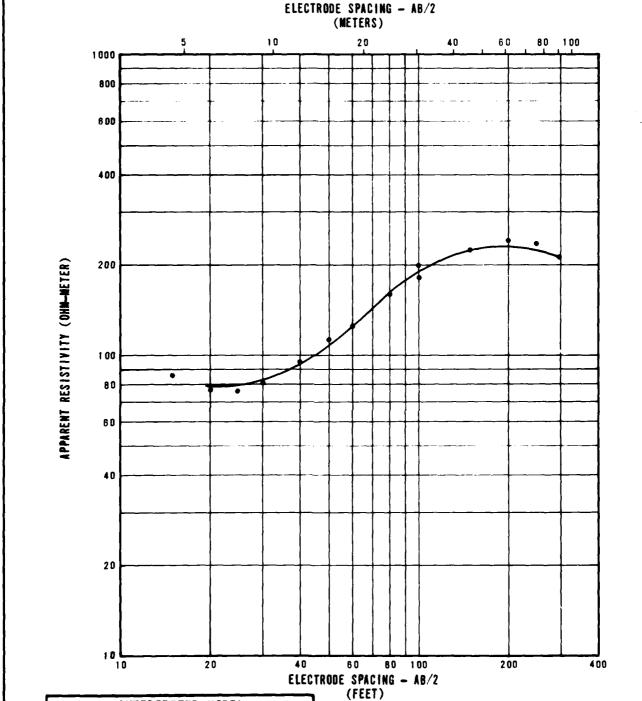


	INTERPRETED MODEL			
LAYE	R DEPTH	RESISTIVITY VALUES		
FEET	METERS	OHM-METER		
0	0	90		
40	12	50		

RESISTIVITY SOUNDING BU-R-9 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER COP, ARIZONA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE

FIGURE 4-8



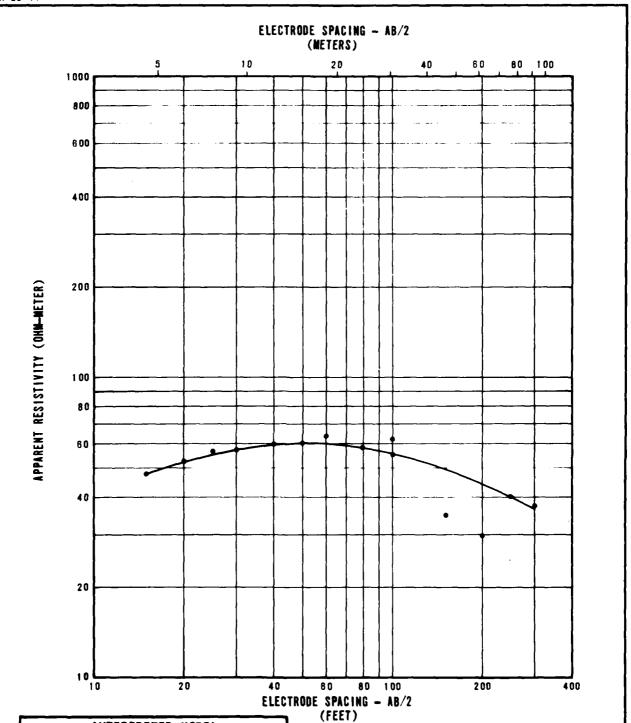
	INTERPRETED MODEL		
LAYE	LAYER DEPTH   RESISTIVITY VAL		
FEET	METERS	OH#-WETER	
0	0	70	
25	8	360	
158	48	40	

RESISTIVITY SOUNDING BU-R-10
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE, BUTLER CDP, ARIZONA

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FIGURE 4-9

UGRO NATIONAL INC.



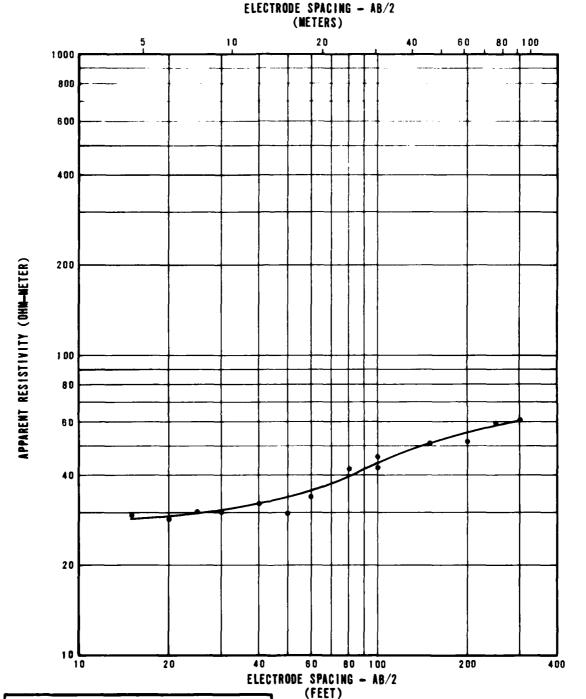
	INTERPRETED MODEL			
LAYE	R DEPTH	RESISTIVITY VALUES		
FEET	METERS	OHM-METER		
0	0	45		
12	4	85		
48	15	30		
	I			

RESISTIVITY SOUNDING BU-R-11 Sounding curve and interpretation Verification site, butler CDP, arizona

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SA

FIGURE 4-10

UGRO NATIONAL INC.



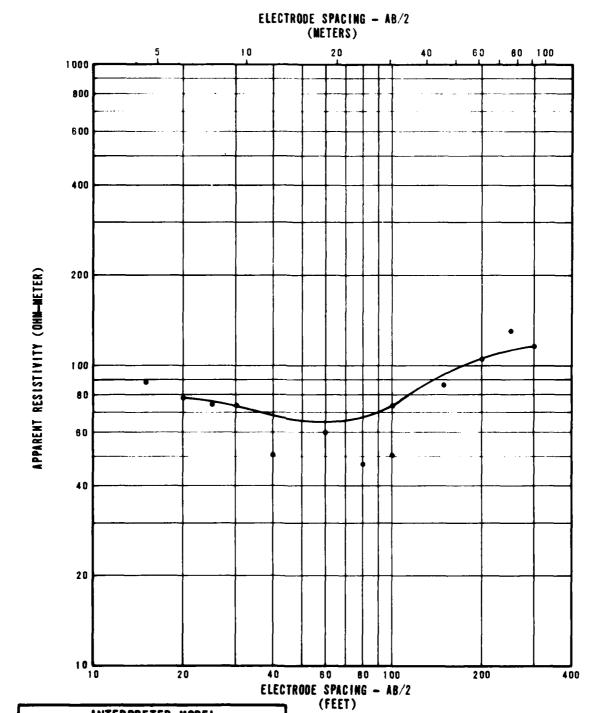
	INTERPRETED MODEL			
LAYE	R DEPTH	RESISTIVITY VALUES		
FEET	METERS	OH#-METER		
0	0	30		
30	8	70		

RESISTIVITY SOUNDING BU-R-12 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP, ARIZONA

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4-11

VERO NATIONAL INC



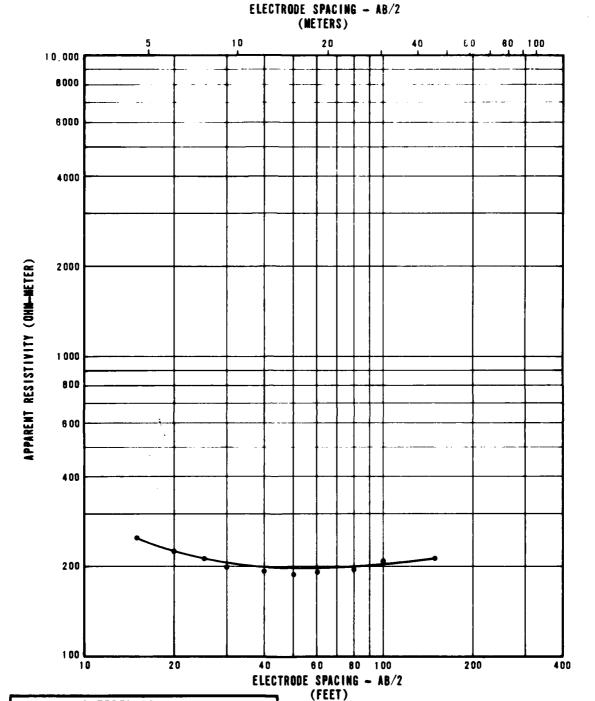
	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	95	
12	4	55	
65	20	170	
		I	

RESISTIVITY SOUNDING BU-R-13 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP. ARIZONA

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4-12

UBRO NATIONAL INC.



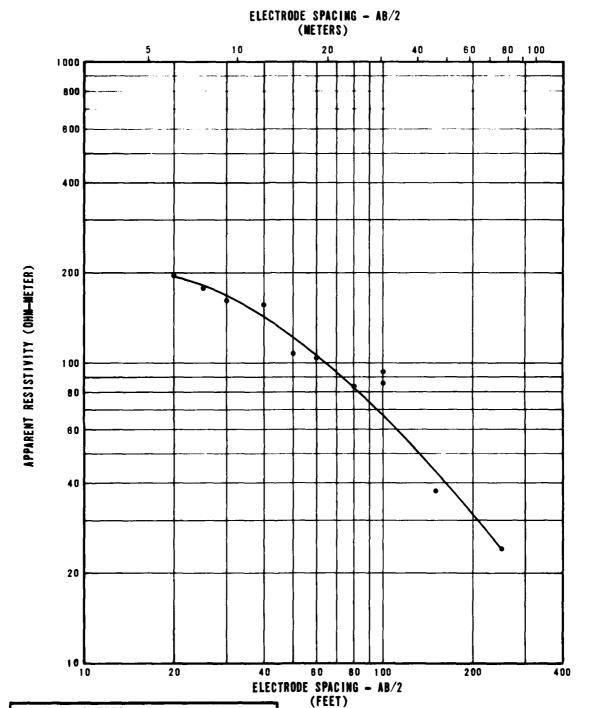
	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHIN-METER
0	0	25
8	2	18
40	12	25

RESISTIVITY SOUNDING BU-R-14
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE, BUTLER COP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

4-13

VORO NATIONAL INC.



	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	2
22	7	55
110	34	11

RESISTIVITY SOUNDING BU-R-15 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, BUTLER CDP. ARIZONA

DEPARTMENT OF THE AIR FORCE SAMSO

4-14

FIGURE

10 AUS 79

AFV-15

SECTION 5.0
GRAVITY DATA

## EXPLANATIONS OF GRAVITY DATA

Gravity data were not available in time (prior to June 1979) for incorporation into this report. A supplemental report containing gravity data and results will be issued at a later date.

SECTION 6.0 BORING LOGS

## EXPLANATIONS OF BORING, TRENCH, AND TEST PIT LOGS

All data from borings, trenches, and test pits are presented on standard Fugro National logs in Sections 6.0 and 7.0. The following explanations are provided as a key to the logs.

A. Designations - Borings, trenches, and test pits are identified as follows:

BU-B-1

BU - abbreviation for the site (e.g., BU-Butler)

- B abbreviation for activity (e.g., B-boring, T-trench, P-test pit)
- 1 number of activity
- B. Sample Type Different sampling techniques were used and the symbols are explained at the bottom of the boring logs. For details of sampling techniques, see Section A5.0 of Appendix A in Volume I. Horizontal lines, to scale, indicate the depth where sampling was attempted.
- C. Percent Recovery The numbers shown represent the ratio (in percent) of the soil sample recovered in the sampler to the full penetration of the sampler.
- D. N Value Corresponds to standard penetration resistance, which is number of blows required to drive a standard split-spoon sampler for the second and third of three 6-inch (15 cm) increments with a 140-pound (63.5 kg) hammer falling 30 inches (76 cm) (ASTM D 1586-67).
- E. Depth Corresponds to depth below ground surface in meters and feet.
- F. Lithology Graphic representation of the soil and rock types.

- G. USCS - Unified Soil Classification System (see Table 6-1 for complete details) symbols.
- Soil Description Except in cases where samples were clas-H. sified based on laboratory test data, the descriptions are based on visual classification. The procedures outlined in ASTM D 2487-69, Classification of Soils for Engineering Purposes, and D 2488-69, Description of Soils (Visual-Manual Procedure) were followed. Solid lines across the column indicate known change in strata at the depth shown.

Definitions of some of the terms and criteria to describe soils and conditions encountered during the exploration follow.

Gradation: A coarse-grained soil is well graded if it has a wide range in grain size and substantial amounts of most intermediate particle sizes.

> Poorly graded indicates that the soil consists predominantly of one size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

Moisture : no feel of moisture

Slightly Moist - much less than normal moisture

Moist normal moisture for soil Very Moist - much greater than normal

moisture

Wet - for soils below the water

table (if known)

Laboratory Chessification Cruters	asia ni	and the	Alectorist Section of the send for the send	inification and and and and and and and and and an		ven und	is es en anima	Attention lamin below "A" lase with PI greater than 7		Onestee See and See See See See See See See See See Se	xapui /	Pasticity	10	0 10 20		Plasticity chart for laboratory classification of fine grained soils	
Information Required for Describing Souls	Give typical name; indicate ap- proximate percentages of and	angularity, surface condition, and hardway of the course	grains, social of geologic harms and other pertinent descriptive information; and symbols in peremisess	rbed soils add infor tratification, degreess,	mossiure conditions and definage characteristics  Example: Silty sand, gravelly; about 20%	heru, unguan grave perices i-in, maximum size; rounded and automotive mand grains coars to day about 16 % non-	plastic fines with low dry strength; well compacted and moist in place; alluvial send;	(MC)			Give typical name; indicate degree and character of plasticity, amount and maximum size of course organs.	condition, odour if any, local or geologic name, and other perti- ment descriptive information, and symbol in parentheses	For undisturbed soils add infor-	mation on structure, stratifica- tion, consistency in undisturbed and remoulded states, moisture	Example:	Clayer sill, brown; slightly plastic; small percentage of	not band; numerous vertical root boles; firm and dry in place; locus; (ML)
Typical Names	Well graded gravels, gravel- and mixtures, little of no fines	Poorly graded gravels, gravel-	Silty gravels, poorly graded gravel-sand-silt mixtures	Clayey gravels, poorly graded gravel-sand-clay mixtures	Well graded sands, f welly sands, little or no fines	Poorly graded sands, gravelly sands, little or no fines	Silty sands, poorly graded sand- salt mixtures	Clayer stads, poorly graded sand-clay mixtures			Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with slight plasticity	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	Organic silts and organic silt- clays of low plasticity	Inorganic silts, micaccous or distomeceous fine tandy or silty soils, clastic silts	Inorganic clays of high plas-	Organic clays of medium to high plasticity	Peat and other highly organic soils
Symbole	à	*5	CM	ပ္ပ	AS S	3.5	SM	SC.	İ		¥	ដ	7	ни	3	ЖО	-
8 8	prain size and substantial all intermediate particle	one size or a range of sizes intermediate sizes missing	ification pro-	n procedures,	frain sizes and substantial all intermediate particle	one size or a range of sizes intermediate sizes missing	es (for identification pro- m ML below)	n procedures.	Her than No. 40 Sieve Size	Toughaess (consistency near plastic limit)	None	Medium	Slight	Slight to medium	High	Slight to medium	and frequently by fibrous
Name Desing fractions	in grain vise as of all intermed		nes (for identification pro-	c Anse (for Identification procedures, CL below)				Phasic fless (for identification procedures, see CL below)		Ditatancy (reaction to shaking)	Quick to slow	None to wery alow	Slow	Slow to	None	None to very slow	
han Jin. and led weights	Wide reage is amounts o	Predominanti with some	Nomphasic Br cedures see	Plastic fines (S	Wide range in amounts of sizes	Predominantly with some	Nonplastic Br cedures, 1	Phastic floors (I	a Fraction Sma	Dry Strength (crushang character- istics)	Nome to slight	Medium to high	Slight to medium	Slight to medium	High to wery high	Medium to high	Readily ident spongy feel lexture
Pink Semilian Procedu (Escheing particles larger than 3 in. and be colimated weights)	20) 20)	herger hieve ison ison ison (litt	Oney table of total of total of total of total of total of total of total of	oM ent ent get	coarse t then sistention, t sient to the se or no series)	fends full of malls nicys al nal clas oquiv Oct	nadi m etion is b.oM	oM eni ) ibnaž iĝ	Mentification Procedures on		yalə bra Jimil biy Q2 qafi (	nii\$			bes to bigging the best of the	NI .	Highly Organic Soils
			ol lon facia s	of mate years 000	Coarse-gray the held of the held has been to held the held to held to held the held t	28.eq	sestian	e son p	noq	volle s el sele svi	SEN 84	o bealers suam to rais GOS W sett)	-ani ilad i aM n	uadi an	×		Ĭ

From Wagner, 1957.

\*\*Boundary charifications. Soils possessing characteristics of two groups are designated by combinations of group symbols. For example CW-GC, well graded gravel-sand mixture with clay blader.

\*\*All serve sizes on this chart are U.S. standard.

\*\*Field Menification Preceder for Pain Grained Soils or Fractions.

\*\*Field Menification Preceder for Pain Grained Soils or Fractions.

These procedures are to be performed on the minus No. 40 serve size particles, approximately 1/4, in. For field classification purposes, screening is not intended.

Different Chambers of the specified state of the court of the characteristic classification purposes, screening is not intended. Dry Strength Chambers of the speciment of the characteristic classification purposes, screening is not intended. Dry Strength Chambers of purposes and several control of the character and passing the other hand several times. A positive reaktion chambers of the appearance of water on the surface of the past which reads and finally it create or crumbles. The rapidity of section and several services of the appearance of water on the surface of the strength of the characters of the appearance of the specimen. The rapidity of section should be seen to see the service of the direct in a soil.

Very Sees class and setting the characters of the specimen. This intending to the characters of the specimen of the characters of the specimen of the specimen of the characters of the specimen of the specimen of the specimen of the specimen of the specimen. The rapidity of section shows a moderately quick reaction.

Foughburs (Consistency mear plassic limis):

After removing particle larger than the No. 40 sieve size, a specimen of soil about once-half inch cube in suze, is mouded to the consistency of pority. If (to off, water mist be added and if sizely, the specimen of soil about once-half inch cube in suze, is mouded to the consistency of pority. If (to off, water mist be added and leaded to the soil by emporation. Then the speciment is roulded out by hand on a smooth surface or between the parms into a thread about one-cital sizely this in manipulation the montaure content is greatedly. During this manipulation the montaure content is greatedly reduced and the speciment suffers deally loses its plassicity, and crumbbig when the passis limit is reached.

After the tread crumbba, the pease should be hamped toperiter and a sight kneading action contained until the lamp crumbbig.

The tougher the thread must be plassic timit and the sight with fraction is the collected of the thread on its plassic timit is discisse either increased could not be thread on its plassic limit indicate either increased clay of the simp when the plassic manipulation to make the plassic clay mad organic clay mad organic clay which organic clay have a very wells and sponsy feel at the plassic limit. simply remove by hand the coarse particles that interfere with the tests.

UNIFIED SOIL CLASSIFICATION SYSTEM

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

6-1 IRO NATIONAL INC.

TABLE

I

Consistency: Consistency descriptions of coarse-grained soils (GW, GP, GM, GC, SW, SP, SM, SC) are as follows.

Consistency	N Value (ASTM D 1586-67)
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	>50

Consistency descriptions of fine-grained soils (ML, CL, MH, CH,) are as follows:

Consistency	Shear (ksf)	Strength (kn/m <sup>2</sup> )	Field Guide
Very Soft	0.25	12	Sample with height equal to twice the diameter, sags under own weight
Soft	0.25- 0.50	12 <b>-</b> 24	Can be squeezed between thumb and forefinger
Firm	0.50- 1.00	24- 48	Can be molded easily with fingers
Stiff	1.00-2.00	48 <b>-</b> 96	Can be imprinted with slight pres- sure from fingers
Very Stiff	2.00- 4.00	96- 192	Can be imprinted with considerable pressure from fingers
Hard	over 4.00	over 192	Cannot be im- printed by fingers

Grain Shape: Angular - particles have sharp edges and relatively plane sides with unpolished surfaces.

Subangular - particles are similar to angular but have somewhat rounded edges.

Subrounded - particles exhibit nearly plane sides but have well-rounded corners and edges.

Rounded - particles have smoothly curved sides and no edges.

Calcareous: Containing calcium carbonate; presence of calcium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid.

Caliche : Soils cemented by porous calcium carbonate and/or other soluble minerals by upward-moving solutions.

Degree of Cementation:

(Stages of development of caliche profile)

Stage	Gravelly Soils	Nongravelly Soils
I	Thin, discontinu- ous pebble coatings	Few filaments or faint coatings
II	Continuous pebble coatings, some interpebble fill-ings	Few to abundant nodules, flakes, filaments
III	Many interpebble fillings	Many nodules and internodular fillings
IV	Laminar horizon overlying plugged horizon	Increasing carbon- ate impregnation

Secondary Material

Example - Sand with trace to some silt

Trace - 5-12% (by dry weight) Little - 13-20% (by dry weight) Some - >20% (by dry weight) Plasticity: Plasticity index is the range of water content, expressed as a percentage of the weight of the oven-dried soil, through which the soil is plastic. It is defined as the liquid limit minus the plastic limit. Descriptive ranges used on the logs include:

Nonplastic (PI, 0 - 4)
Slightly Plastic (PI, 4 - 15)
Medium Plastic (PI, 15 - 30)
Highly Plastic (PI, >30)

Cobbles and Boulders

A cobble is a rock fragment, usually rounded by weathering or abrasion, with an average diameter ranging between 3 and 12 inches (8 and 30 cm).

A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (30 cm) or more.

- I. Remarks This column was provided on boring and trench logs for comments regarding drilling difficulty, number and size of cobbles or boulders encountered, trench wall stability, loss of drilling fluid in the boring, and other conditions encountered during drilling and excavations.
- J. Dry Density and Moisture Content The boring logs include a graphical display of laboratory test results for dry density (ASTM D 2937-71) in pounds per cubic foot and kilograms cubic meter and moisture content (ASTM D 2216-71) in percent from representative samples taken during drilling. The symbols are explained at the bottom of the boring logs.

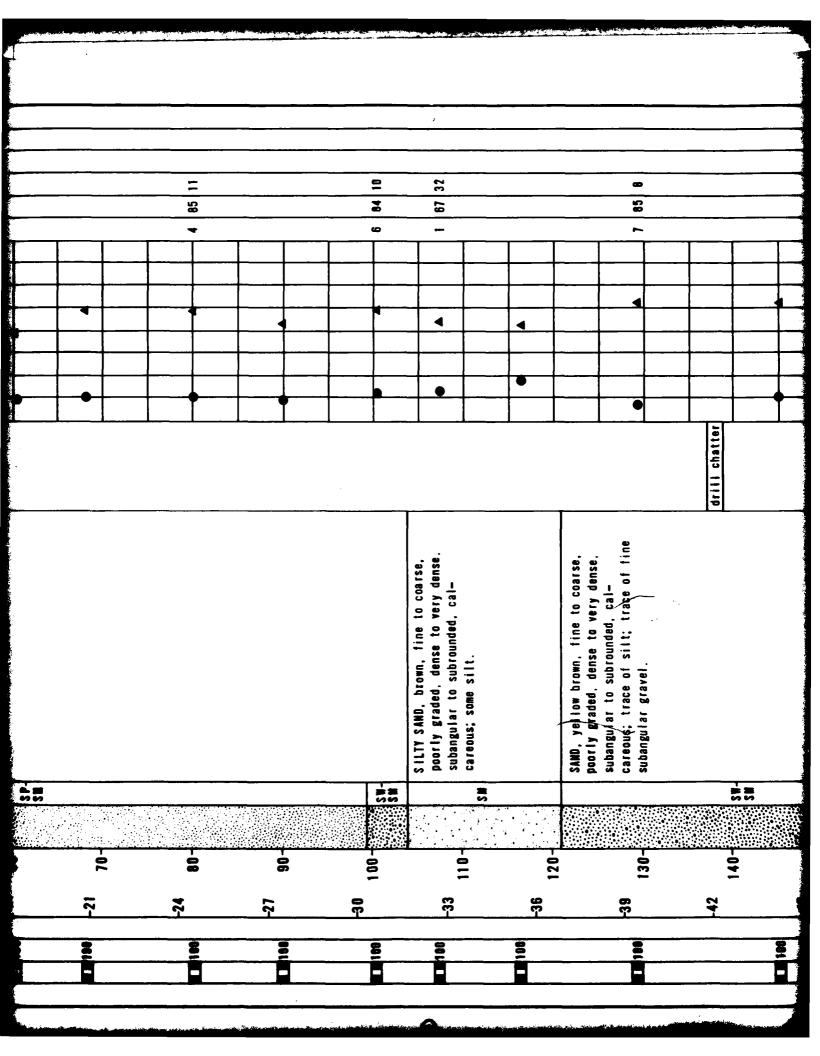
- K. Seive Analysis The numbers represent the percentage by dry weight (ASTM D 422-63) of each of the following soil components:
  - GR Gravel, rock particles that will pass a 3-inch (76 mm) sieve and are retained on No. 4 (4.75 mm) sieve.
  - SA Sand, soil particles passing No. 4 sieve and retained on No. 200 (0.075 mm) sieve.
  - FI Fines, silt or clay, soil particles passing No. 200 sieve.
- L. Atterberg Limits (LL and PI) -
  - LL Liquid Limit, the water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
  - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
  - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soilwater mixture is plastic.
  - NP Nonplastic.
- M. Miscellaneous Information -
  - Elevations indicated elevations on the logs are estimated from topographic maps of the study area, within an accuracy of half the contour interval.
  - Surficial
    Geologic Unit indicates the surficial geologic unit in which the activity is located.
  - Date Drilled indicates the period from beginning to completion of the activity.
  - Drilling

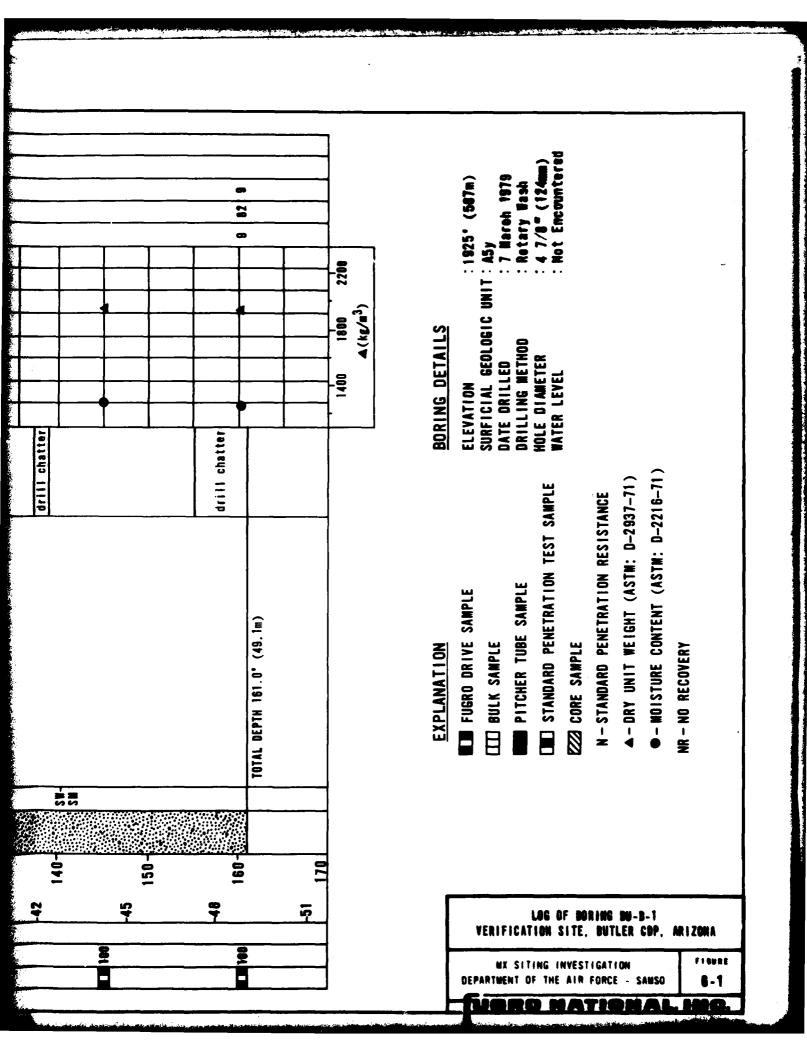
    Method signifies the type of drilling procedure used such as rotary wash.
  - Hole Diameter nominal size of boring drilled.
  - Water Level indicates depth from ground surface to water table where encountered.

Trench Length - length at ground surface of final trench excavation.

Trench
Orientation - bearing of longitudinal trench centerline.

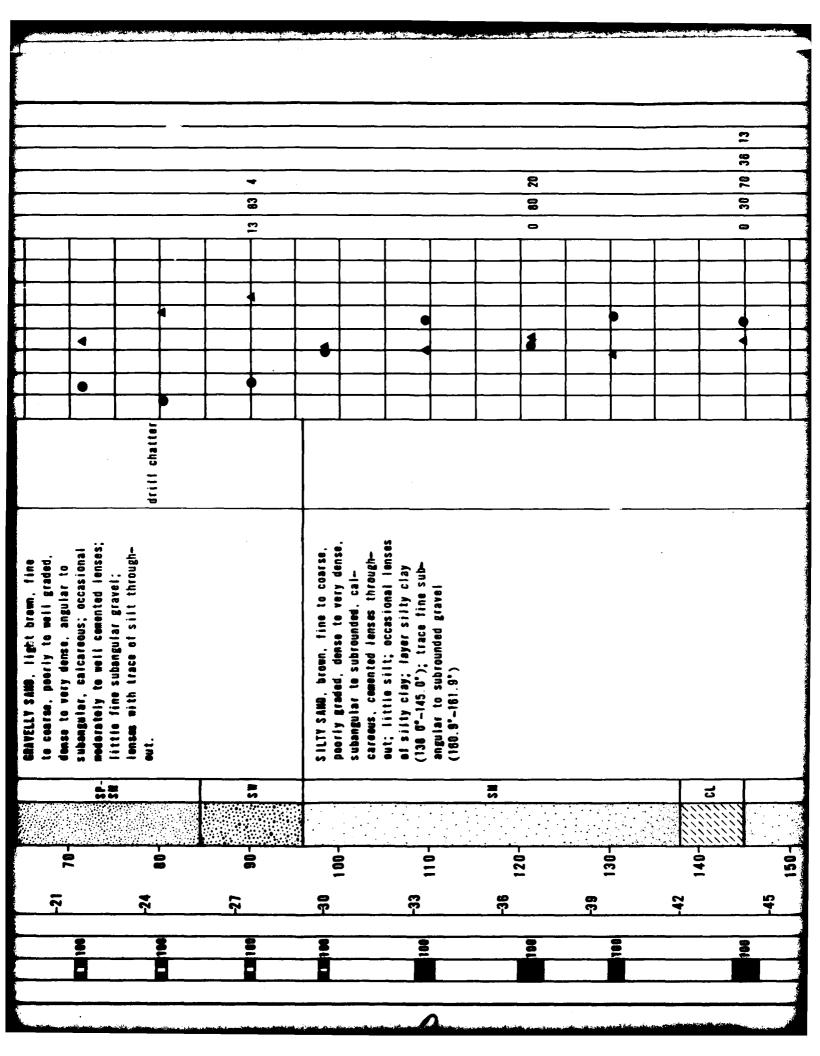
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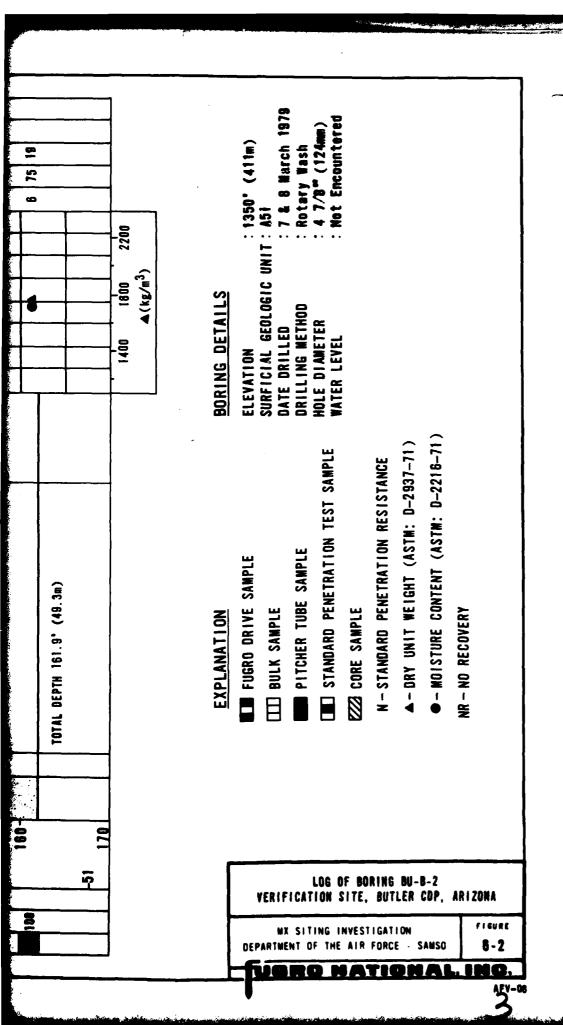




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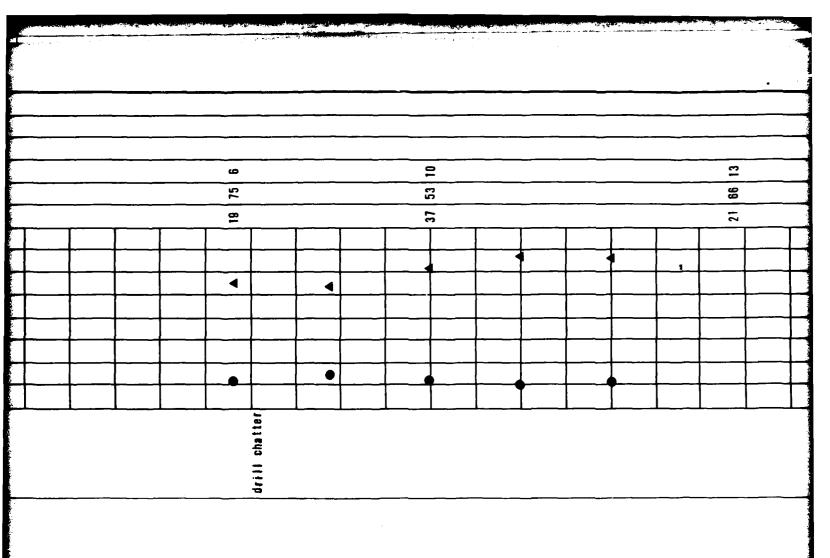
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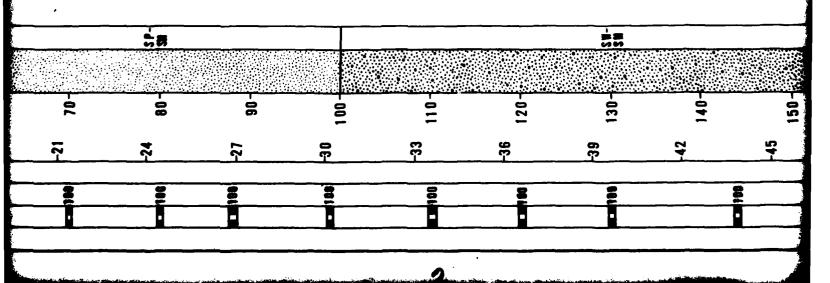


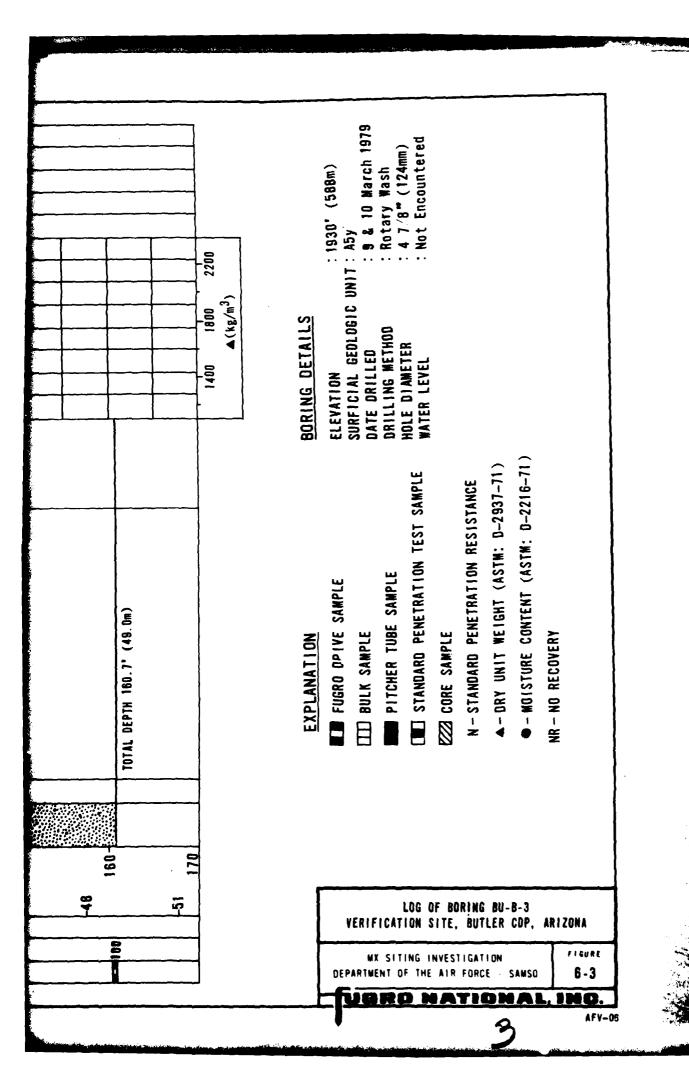


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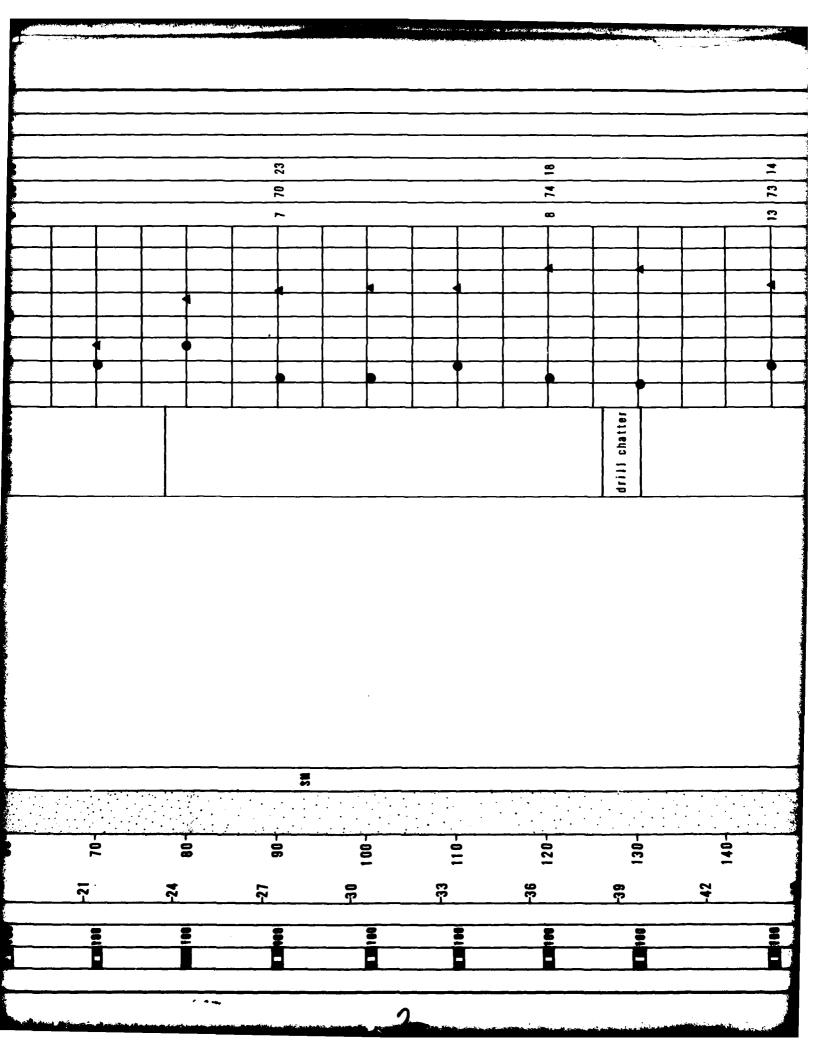
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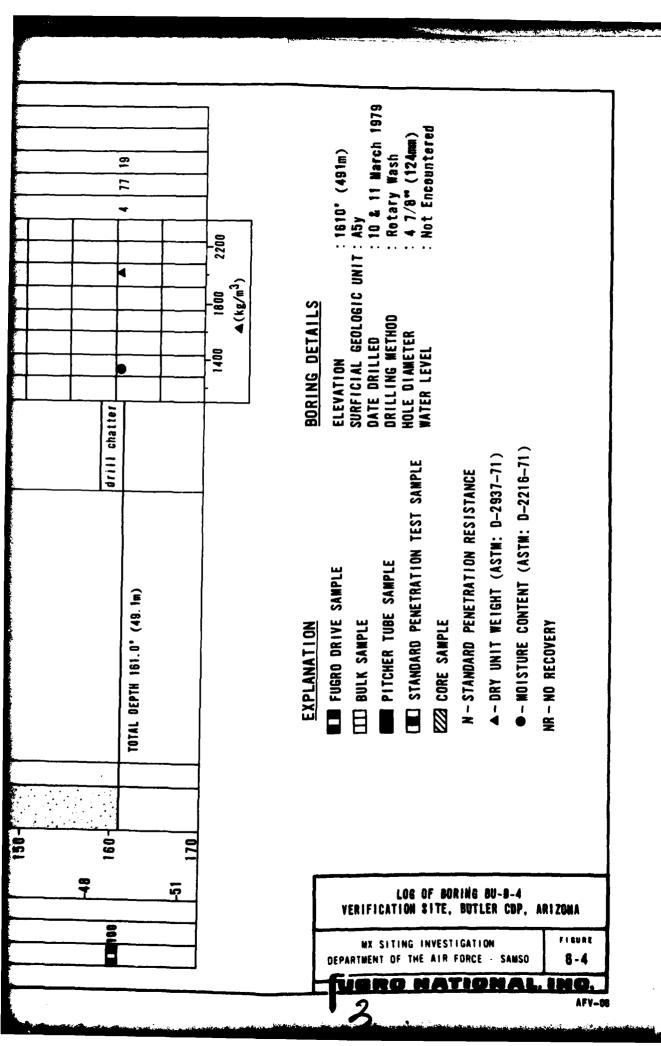






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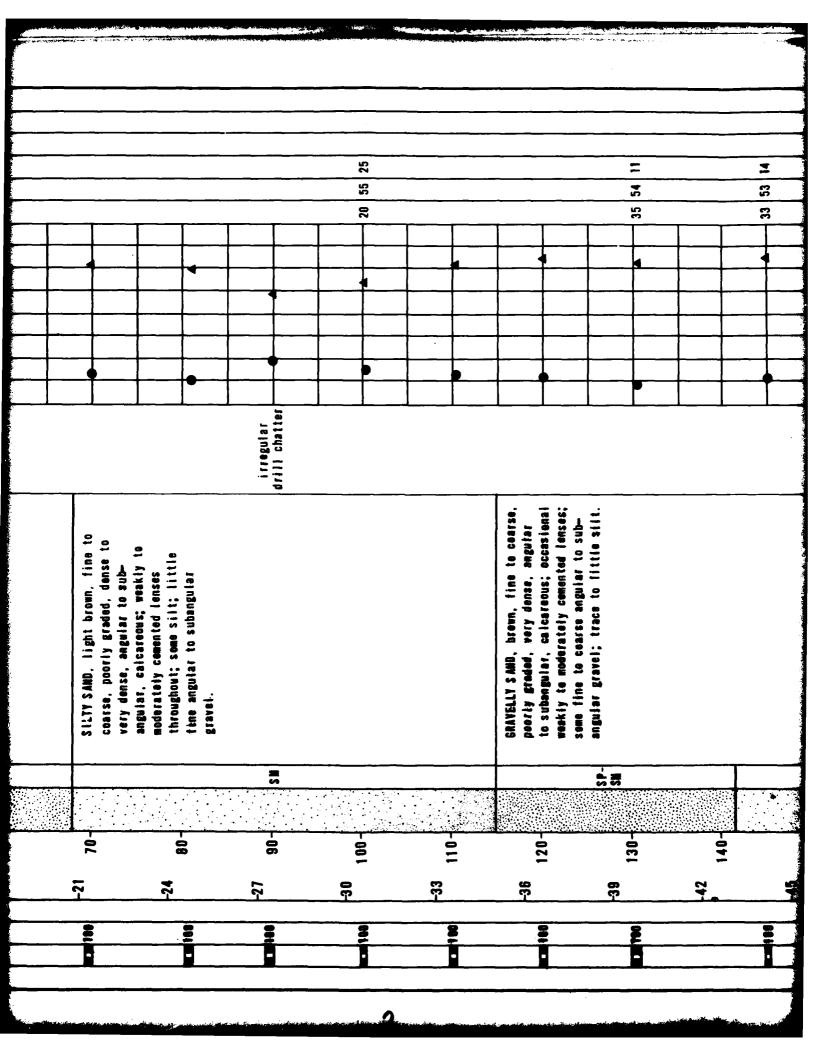


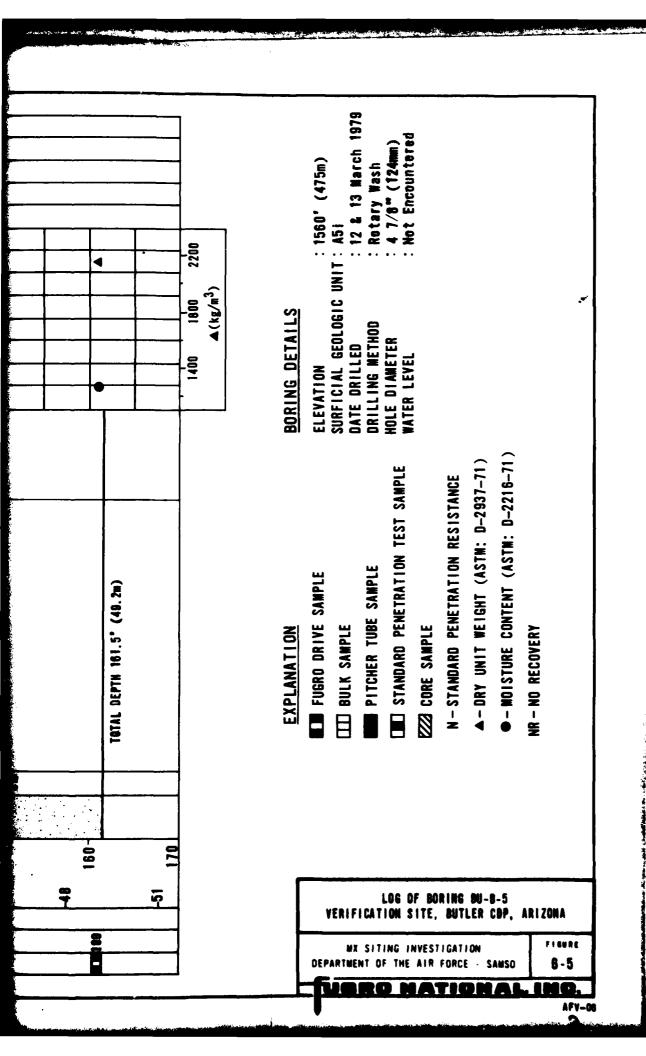


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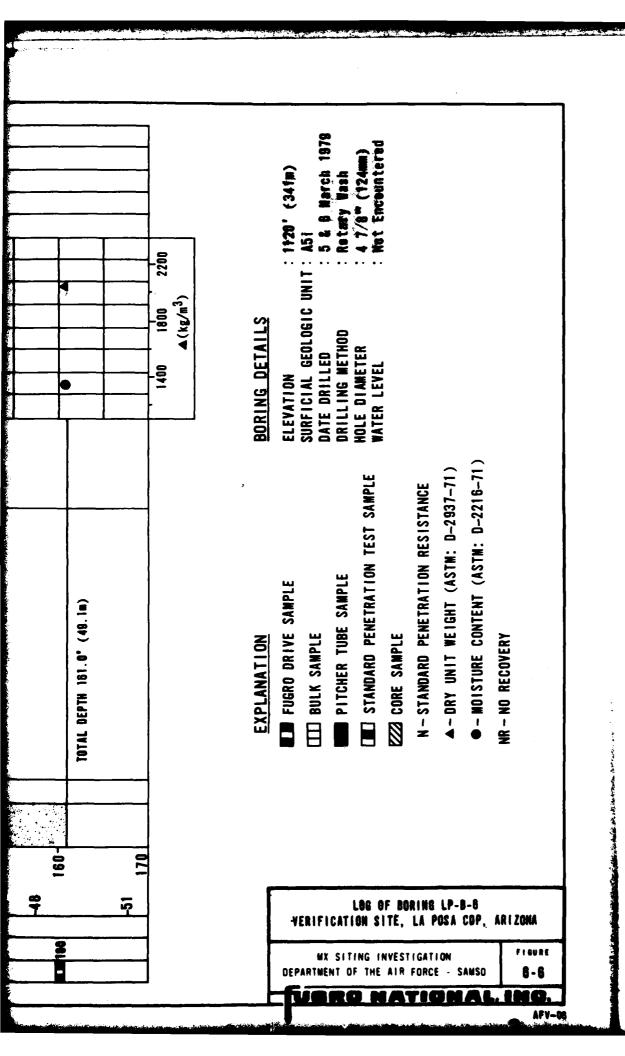
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2	_		;	t =	che ine	_	<b>→</b> 0	<u>~</u>					
NOTE DESCRIPTION		interbedded tayers of GRAVEL and	SAND: Gravel:	fine to coarse, ell graded, dense	vory dense, angular to sub- rounded, calcareous; some caliche development on gravels; some fine	to coarse angular to subrounded sand; trace to little silt.	GRAVELLY SAND (SM and SW): light brown, fine to coarse, poorly to	well graded, medium dense to very dense, angular to subrounded, calcareous; some fine to coarse	angular to subrounded gravel; trace to some silt				
		SM interbedded layers of GRAVEL and		GRAVEL (GP-GM, GM and G rown, fine to coarse, to well graded, dense	rounded, calcareous; some cali	sand; trace to little silt.	GRAVELLY SAND (SM and SM): ligh brown, fine to coarse, poorly t	dense, angular to subrounded,	angular to subrounded gravel;		*		
	sn	<del>  </del>	SAND: GRAYEL:	SANDY GRAVEL (GP-GM, GM and GM); brown, fine to coarse, poorly to well graded, dense	rounded, calcareous; some cali	77	GRAVELLY SAND (SM and SW): ligh	dense, angular to subrounded, calcareous; some fine to coarse	angular to subrounded gravel; trace to some silt		*		
C2 Droea	sn	<del>  </del>	SAND: GRAYEL:	SANDY GRAVEL (GP-GM, GM and GM); brown, fine to coarse, poorly to well graded, dense	rounded, ca		GRAVELLY SAND (SM and SW): ligh		angular to trace to so			20	
C2 000000	FEET LITHOUS US	8	SAND: GRAYEL:	SANDY GRAVEL (GP-GM, GM and Google, GM and Google, GM); brown, fine to coarse, or or or or or or or or or or or or or	rounded, ca	500000000000000000000000000000000000000		000000 0000000 00000000000000000000000	angular to trace to so	9			
SO TO EA	METERS FEET LITHE US	8	SAND: GRAYEL:	10 000 GP GR GMD; brown, fine to coarse, poorly to well graded, dense	rounded, ca				angular to trace to so			-09	
C2 000000	METERS FEET LITHO US	0	SAND: GRAYEL:	10 000 GP GR GMD; brown, fine to coarse, poorly to well graded, dense	rounded, ca	500000000000000000000000000000000000000		000000 0000000 00000000000000000000000	angular to trace to so	9			

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82	8	55 55	2			4			2		
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		1				<u></u>	+		4		
	+	+ +			-	<u> </u>	+	<del></del>	+		
	9										
		•									
	SILTY SAND, brown, fine to coarse, goorly graded, dense to very dense, angular to subrounded, calcareous; occasional weak to moderately comented lenses; little to some	silt; trace to some gravel.									
						8					
	[										
2	2	06	8		- - - -	120-	130		9	200	
<b>Z</b>	- Ba - 17				•			77	<del> </del>	150	
<u> </u>	<b>5</b>		30 100-			-36	-39		140		
<u> </u>	<b>6</b>		100		•	120-	130-		<del> </del>		



SECTION 7.0
TRENCH AND TEST PIT LOGS

# EXPLANATION OF TRENCH AND TEST PIT LOGS

See Section 6.0, "Boring Log", for explanations.

BULK SAMPLE	HETERS 30	PTH	LI THOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMA	ARKS	AN	IEV	SIS		<b>.</b> –
3			<u> </u>		5				GR	SA	FI	ш	PI
	0	2 -		SM	medium dense	SILTY SAND, light brown to brown, fine to coarse, poorly graded, dry to slightly moist, angular, calcareous; little silt (0.0'-3.5'); some silt (4.0'-10.0'); layer of clayey sand (3.5'-4.0'), stage II caliche (4.0'-10.0').	vertica caving	l walls slightly		84	15		
ΗТ	- 1		111111	SC			<del>                                     </del>		4	49	47	30	16
		6 -											
	- 2	8 -		SM	dense			tical stable					
	<b>-</b> 3	10-		SP-		GRAVELLY SAND, light brown, fine to coarse, poorly graded, dry, sub-angular, calcareous; little to some fine subangular gravel; trace silt.							
	- 4												
		14-				TOTAL DEPTH 14.0' (4.3m)		<u> </u>					
	<b>–</b> 5	16-											
		18-											
	- 6	20-						:					
								i					

# TRENCH DETAILS

SURFACE ELEVATION : 1810' (491m)
DATE EXCAVATED : 8 MARCH 1979

SURFICIAL GEOLOGIC UNIT: A5y

TRENCH LENGTH : 18' (4.9m)
TRENCH ORIENTATION : NE-SW

LOG OF TRENCH BU-T-1 VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-1

**USRO NATIONAL INC.** 

BULK SAMPLE	METERS A	FEET HA	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REM	ARKS	AN	A LY	<b>3</b>   <b>S</b>	
100	0	0	<b>3</b>		NOO	GRAVELLY SAND, brown, fine to coarse, poorly graded, dry, angular to sub-angular, calcareous; fine to coarse, some subangular to subrounded gravel;					F1	•
	- i	2-		SM		trace to fittle silt; occasional cobbles to 11" size; stage I caliche (3.0'-6.0').						
	- 2	8 -			dense		ver waits	tical stable				
	- 3	10-		SP- SM	 							
	-4	14-				TOTAL DEPTH 14.0° (4.3m)	,					
	- 5	16								<u>.</u>		
		18-										
	- 6	20-										

SURFACE ELEVATION : 1930' (588m)
DATE EXCAVATED : 8 MARCH 1979

SURFICIAL GEOLOGIC UNIT: A5y

TRENCH LENGTH : 18' (4.9m)

TRENCH ORIENTATION : E-W

LOG OF TRENCH BU-T-2 VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

FIGURE 7-2

TUBRO NATIONAL INC.

BULK SAMPLE	WETERS A	FET KI	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMA	RKS	1	IEV ALY:			
BUL	0	<u> </u>	3		NO 0		<del>                                     </del>	<del></del>	GR	SA	FI	LL	P
	- 1	2		SP- SM	medium dense	SAND, light brown, fine to coarse, poorly graded, slightly moist, sub-angular, calcareous; trace silt	vert walls	icaí caving	1	91	6		
	- 2	8 -				GRAVELLY SAND, red brown, fine to			4.1	52	7		×
	- 3	8		! !		coarse, well graded, dry, sub- angular, calcareous; some fine to coarse subangular gravel; trace silt; stage 1 caliche (9.0'-14.0').	vert walls	ical stable		J2			
		12-		SW-	dense								
	- 4	14-				TOTAL DEPTH 14.0' (4.3m)	<b> </b>	· · · · · · · · · · · · · · · · · · ·					
	- 5	16-										] } }	
		18-											
	- 6	20-		 								ļ !	

SURFACE ELEVATION : 1425' (434m)
DATE EXCAVATED : 12 MARCH 1979

SURFICIAL GEOLOGIC UNIT: A5y/A1

TRENCH LENGTH : 18' (4 9m)
TRENCH ORIENTATION : N-S

LOG OF TRENCH BU-T-3 VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-3

VORO NATIONAL INC.

DEFIN AND SOUTH THE PROPERTY OF THE PROPERTY O	I SAMD, FIRM GIOWN, TIME TO COLISE,		15		F1	PI
SM sm med den	coarse, poorly graded, dry, sub- angular, calcareous; some silt; little fine to coarse subangular gravel.  SAND, light brown, fine to coarse,		15	51	34	
4 - med den	I SAMD, FIRM GIOWN, TIME TO COLISE,	-	1			
6 - SM	poorly graded, slightly moist, sub- angular, calcareous; trace fine subangular gravel; trace silt	vertical walls stable				
3 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10			0	35	65	
12- SM den	SILTY SAND, brown, fine to coarse, poorly graded, dry, subangular; some silt.					
14	TOTAL DEPTH 14.0' (4.3m)	<del> </del>				
-5						
18-						
- 8 20-						

SURFACE ELEVATION : 1350' (411m)
DATE EXCAVATED : 12 MARCH 1979

SURFICIAL GEOLOGIC UNIT: A51

TRENCH LENGTH : 18' (4 9m)

TRENCH ORIENTATION : E-W

LOG OF TRENCH BU-T-4
VERIFICATION SITE, BUTLER CDP, ARIZONA

MX STITMS INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7 - 4

VERO NATIONAL INC.

BULK SAMPLE	METERS TO	PTH LEL	LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REM	ARKS	AN	IEV ALY:	SIS		
2			5		5				GR	SA	FI	1	P
	0	2 -		SM	medit dense	SILTY SAND, light brown, fine to coarse, poorly graded, dry, sub-angular, calcireous; little to some silt; trace fine subangular gravel;			4	69	27		
	1							İ	9	78	13		Ì
ш		4 -			<u> </u>		- var	i tical					ĺ
	- 2	6 -		SP-	medium dense	SAND, light brown, fine to coarse, poorly graded, dry, subangular, calcareous; trace fine subangular gravel; trace silt; stage III caliche (6.5'-10.0').	watis	stable					
		8-		<b>-</b>					 				
	- 3	10-				TOTAL DEPTH 10.0' (3.0m)		Y		]			
		12-											
	- 4						į		}				
ĺ		14-											
-													
	- 5	18~		:									
		18-										İ	
					}								
	- 6	20-											
										[			
													l

SURFACE ELEVATION : 1925' (587m)
DATE EXCAVATED : 13 MARCH 1979

SURFICIAL GEOLOGIC UNIT: A5y

TRENCH LENGTH : 16' (4 9m)

TRENCH ORIENTATION : NW-SE

LOG OF TRENCH BU-T-5
VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAWSD

7-5

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BULK SAMPLE	BE TERS	FEET HIGH	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	SIEVE ANALYSIS	
76	0	2	<b>1</b>	SM	medium dense	Sility SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some silt; trace fine angular to subangular gravel; stage II caliche (4.0'-5.0')	vertical walls caving slightly	GR SA FI	LLPI
	- 1 -	5 -			dense	TOTAL DEPTH 5.0° (1.5m)			
SURF	IC IA	L GE	ATION: 1350' Ologic Unit:	(41) A5y	I#)	LOG OF TEST PIT BU-P-1			
	-	2 - 3 - 4 -		SM	medium dense	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; little silt; little fine to coarse angular gravel	vertical walls stable		
		5 -				TOTAL DEPTH 5.0' (1.5m)	<u> </u>	111	
SURF SURF	A CE I C I A	E LEV	ATION: 1880' DLOGIC UNIT:	(512 A5i	(m.)	LOG OF TEST PIT BU-P-2			
							EST PITS BU-P- On Site, Butles		
						DEPARTMENT OF	IG INVESTIGATION THE AIR FORCE	SAMSO	Fieun 7-6
AUG 7						MX SITIN	IG INVESTIGATION	SAMSO	FI 7

BULK SAMPLE	DE PTH	9076	USCS	ONSISTENCY	SOIL DESCRIPTION	REM	ARKS	1 -	IEV ALY:	-		
				<b>8</b>		l		GR	SA	FI	ιι	P
	1		SM	medium dense	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; little silt, trace fine angular gravel.		tical stable					
	2 3 1		SW- SM	dense	SAND, light brown, fine to coarse, well graded, dry, angular, calcareous; trace silt; trace fine angular gravel.	vertica	al walls slightly		88	7		
LUBEAC	5 F <b>F</b> 1F	VATION: 1800*	(54)	3m )	TOTAL DEPTH 5.0' (1.5m)				_	L_	L	L
URFIC	IAL E	EOLOGIC UNIT	: A5y	J /	LOG OF TEST PIT BU-P-3							
	) 0	-	CL	firm	SANDY CLAY, brown, slightly moist, slightly plastic, calcareous; some fine to medium subangular sand.			2	47	51	26	1
	1 2	-	CL	firm medium dense	slightly plastic, calcareous; some	1	tical stable	2	47	51	26	1
	2 3 4			med i um	slightly plastic, calcareous; some fine to medium subangular sand.  SILTY SAND, brown, fine to coarse, peorly graded, slightly moist, angular, calcareous; some silt;	walls		2	47	51	26	1
	1 2 2 3 1 4 4 5 5		SM SP-	medium dense dense	slightly plastic, calcareous; some fine to medium subangular sand:  SILTY SAND, brown, fine to coarse, peorly graded, slightly moist, angular, calcareous; some silt; trace fine subangular gravel.  SAND, light brown, fine, poorly graded,	walls		2	47	51	26	3
	1 2 2 3 1 4 4 5 5		SM SP-	medium dense dense	slightly plastic, calcareous; some fine to medium subangular sand.  SILTY SAND, brown, fine to coarse, peorly graded, slightly moist, angular, calcareous; some sift; trace fine subangular gravel.  SAND, light brown, fine, poorly graded, dry, angular, calcareous; trace silt.	walls		2	47	51	26	3
	1 2 2 3 1 4 4 5 5		SM SP-	medium dense dense	slightly plastic, calcareous; some fine to medium subangular sand.  SILTY SAND, brown, fine to coarse, peorly graded, slightly moist, angular, calcareous; some sift; trace fine subangular gravel.  SAND, light brown, fine, poorly graded, dry, angular, calcareous; trace silt.	EST PIT	S BU-P-3	A		BU -	P-4	

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<b>⊑</b>   ```	PTH	L067	uscs	C ONSISTENCY	SOIL DESCRIPTION	REMA			SIEVI	_		
ULK SAN	FEET	LITHOLOGY	S	MSIS	SUIL DESCRIPTION	KEMA	·KV2		ALYS			Τ,
0	0			medium dense	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some silt; stage III caliche (2.8°-4 5°).			GR 1	SA	FI		<b>F</b>
- 1	3 –		SM				tical stable					
	4 -			dense								
r	5 -	1	1		TOTAL DEPTH 5.0' (1.5m)	<b>_</b>		-	1		'	
0	0	VATION: 1510' EOLOGIC UNIT:	Auy	AJU	GRAVELLY SAND, light brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some fine to coarse subangular gravel; some silty	1						
	2 -		\$ S		clay; stage i caliche (1.0'-2 5')	Ver	tical	32	47	21		
-1	3 -	37777	em	medium dense	SILTY SAND, light brown, fine to coarse, poorly graded, dry, subangular, calcareous; some silt; trace fine subangular gravel; disseminated caliche (2.5°-5.0°)	walls	stable					
	4-		SM									
-DEACE		(AT 10N: 1580'	1 (47)	<u></u>	TOTAL DEPTH 5.0° (1.5m)				للا	Ш	<u>_</u>	T
RFICIA	LGE	EOLOGIC UNIT:	A5 i	m,	LOG OF TEST PIT BU-P-6  LOGS OF TE							<u> </u>

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FIGURE

7-8

NATIONAL INC.

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

BULK SAMPLE	METERS A	FEET	LITHOLOGY	nscs	ONSISTENCY	SOIL DESCRIPTION	REMARKS	1	IEV ALY:		
198	0	0 1 -		sc	medium dense	GRAVELLY SAND, fight brown, fine to coarse, poorly graded, dry, sub-angular, calcareous; some fine to coarse subangular gravel; little silty clay (0.0°-3.2'); trace silty clay (3.2°-5.0'); stage II caliche (3.0°-5.0').	vertical		45		
	 	3 -		SP- SC	dense		walls stable				
			ATION: 1680' OLOGIC UNIT		(11)	TOTAL DEPTH 5.0' (1.5m) LOG OF TEST PIT BU-P-7		1_	<u> </u>		
	0	0				SILTY SAND, brown, fine to coarse,	1	T			
	0	1 -		SM	med i um	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some sitt; trace fine angular gravel.	vertical walls caving				
	-1	0 1 - 2 - 3 -		SM SP- SM	medium dense	poorly graded, slightly moist, angular, calcareous; some silt;					
	-1	3 -		SP-		poorly graded, slightly moist, angular, calcareous; some silt; trace fine angular gravel.  SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; trace silt; trace fine angular gravel.					
SURF	-1	3 - 4 - 5 -	AT 10N : 1580	SP- SM	dense	poorly graded, slightly moist, angular, calcareous; some silt; trace fine angular gravel.  SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; trace silt; trace fine angular gravel					
SURFF	-1	3 - 4 - 5 -		SP- SM	dense	poorly graded, slightly moist, angular, calcareous; some silt; trace fine angular gravel.  SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; trace silt; trace fine angular gravel  TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT BU-P-8					

	DEPTH	V 90.	S	ENCY				1 '	IEV		
BULK SAMPLE	METERS Feet	LITHOLOGY	nscs	C OWS! STENCY	SOIL DESCRIPTION	REM	ARKS	L	A LYS		L
	0 0 1 - 2 3 - 1		ML	firm	SANDY SILT, brown, slightly moist, slightly plastic, calcareous; some fine to medium angular sand	ver walls	tical stable	GR	SA	FI	LL PI
SURFA	5 O O	VATION: 1710' EOLOGIC UNIT:	(521 A5y	m)	TOTAL DEPTH 5.0° (1.5m)  LOG OF TEST PIT BU-P-9  SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some silt; little fine to coarse subangular gravel.	7		17	58	25	NF
Щ	2	1	SM	medium dense		ļ					
	-1 4	20,000			SAMBY CRAVEL brown fine to coarse		tical stable				
		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	GM	dense	SANDY GRAVEL, brown, fine to coarse, poorly graded, slightly moist, sub-angular, calcareous; some fine to coarse subangular sand; little silt.						
RURFA	- 1 4 - 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(555		poorly graded, slightly moist, sub- angular, calcareous; some fine to						
SURFA	- 1 4 - 5	20 40 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(555		poorly graded, slightly moist, sub- angular, calcareous; some fine to coarse subangular sand; little silt. TOTAL DEPTH 5.0° (1.5m)	walls	stable	AN	D 8	BU - I	P-10 ZONA

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BULK SAMPLE	ME TERS TO	FEET	LITHOLOGY	SOSA	CONSISTENCY	SOIL DESCRIPTION	REMARKS	SIEVE AMALYSIS GR SA F	<u>i</u>
	0	1 -		SP- SM	medir dense	SAND, brown, fine to coarse, poorly graded, slightly moist, subengular, calcareous; trace silt; trace fine subangular gravel.	vertical walls stable		
	    -  -	3 -		CL	stiff	SANDY CLAY, red brown, slightly moist, medium plastic, calcareous; some fine to coarse angular sand; trace of subangular gravel; stage II caliche (2.0'-3.25'), stage III caliche (3.25'-3.5').			
		4				TOTAL DEPTH 3.5' (1.1m)	cementation at 3.5° exceeded capacity of Case 580C backhoe		
		5 -		(21.2					
URF	ICIA	L GE	ATION: 2030' Ologic Unit:	(619 : A5i	M <i>)</i>	LOG OF TEST PIT BU-P-11			
	0	1 -		SM	medium dense	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; little silt; trace fine angular gravel.	vertical walls stable		
	  -     	3 -		sc		CLAYEY SAND, brown, fine to coarse, poorly graded, slightly moist, angular, calcareous; some silty clay; trace fine angular gravel.			
			///////			TOTAL DEPTH 5.0' (1.5m)	<u> </u>		1 1 1
		5 -		<u> </u>					
URF	ACE I	5 - ELEV	ATION:1930' Ologic Unit:	(588 A5y	<b>m</b> )	LOG OF TEST PIT BU-P-12		_	
URF	ACE I	5 - ELEV	ATIOM:1930° Ologic unit:	(588 (588 A5y	m)	LOGS OF 1	EST PITS BU-P-1 ION SITE, BUTLER		

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BULK SAMPLE	DEPTH	9070	nscs	C ONS! STENCY	SOIL DESCRIPTION	REMARKS		S IEVI IA LY S	- 1		
	_	– .	<b>_</b> '	<b>3</b>			GR	SA	FI	LL	P
-1	2 -	-	SM	medium dense	SILTY SAND, brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some silt.	vertical walls stable					
SURFACE SURFICI		VATION: 1770' EDLOGIC UNIT:	(534 : A5y	9m)	TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT BU-P-15  SANDY GRAVEL, red brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous;			33			
-1	2 -		GM	dense	fittle fine to coarse subangular sand; little silty clay (0.0'-1.5'); little silt (1.5'-5.0'); occasional cobbles to 10" size throughout.	vertical walls stable					
URFACE URFICT	5 ELEI	YATION: 1840 'EOLOGIC UNIT:	(56 A5 i	in)	TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT BU-P-16	TEST PITS BU-P-1				P-1	

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MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

<u>≅</u>	DEPTH	LITHOLOGY	SOSA	ONSISTENCY	SOIL DESCRIPTION	REMA	RKS		IEV ALY	_	
		=		800				GR	SA	FI	LLP
	1.		SM	medium dens	SILTY SAND, light brown, fine to medium, poorly graded, slightly moist, subangular, calcareous; some silt.		ical	2	73	25	
	3 - 1		CL	firm	SANDY CLAY, light brown, slightly moist, slightly plastic, calcareous; some fine to coarse subangular sand; trace fine sub-rounded gravel.  GRAVELLY SAND, light brown, fine to		stable				
		///////	SP-	medium	coarse, poorly graded, dry, sub- angular, calcareous; some fine sub-						
F	5 -		SM	dense	angular gravel; trace silt.	<u> </u>		1			
HDEAC	E FIEV	ATION: 1895'	(57)	3.	TOTAL DEPTH 5.0' (1.5m)	1,		_	L.	<u> </u>	
7	0				GRAVELLY SAND, light brown, fine to	1		T			
	2 -		SM	medium dense	GRAVELLY SAND, light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fine subangular gravel; little silt.	,	ical stable	24	58	18	
	1 •		SM 62-		coarse, poorly graded, slightly moist, subangular, calcareous; some	,		24	58	18	
	1 · · · · · · · · · · · · · · · · · · ·		62- GM	medium dense	coarse, poorly graded, slightly moist, subangular, calcareous; some fine subangular gravel; little silt.  SANDY GRAVEL, light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fine to coarse sub-	,		24	58	18	
TT-	1 - 2 - 3 - 4 - 5 - E ELEV	ATION: 2045' OLOGIC UNIT:	G?- GM	medium dense	coarse, poorly graded, slightly moist, subangular, calcareous; some fine subangular gravel; little silt.  SANDY GRAVEL, light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fine to coarse subangular sand; trace silt.	EST PITS	Stable  BU-P-1	7 AI		BU -	

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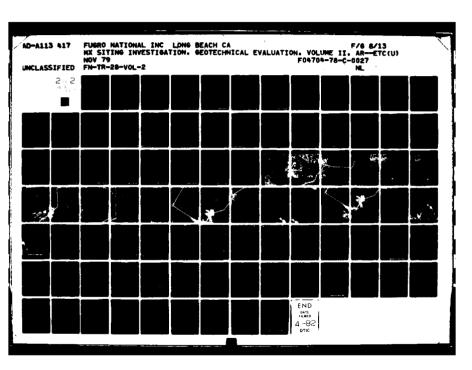
BULK SAMPLE	WE TERS	FEET #19	LITHOLOGY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	ANA	LYS SA	ıs	LL	P
	0	1 -		CL	firm	SANDY CLAY, light brown, slightly moist, slightly plastic, cal—careous; some fine to coarse sub—angular sand; little subangular gravel; occasional cobbles to 8 " size.	vertical walls stable					
	1	3 -		SP- SM	dense	GRAVELLY SAND, light brown, fine to coarse, poorly graded, dry, sub— angular, calcareous; some fine to coarse subangular gravel; trace silt; occasional cobbles.						
		5 -				TOTAL DEPTH 4.0' (1.2m)	refusal of Case 580C backhoe at 4.0 on boulders					
URF	ACE	ELEV	ATION: 2170'	(88	1m)					_		
URF	ICIA	L GE	OLOGIC UNIT:	A5i		LOG OF TEST PIT BU-P-19						
	1	2 3		GP- GM	medium dense	SANDY GRAVEL, brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fine to coarse subangular sand; trace silt; occasional cobbles to 5" size throughout.	vertical walls stable	45	44	11		
									-	ł		
ILDE.	ACE C	D T	T 104 · 2280 ·	(895		TOTAL DEPTH 5.0' (1.5m)	J	11				L
URF	ICIAI	GE	ATION: 2280' Dlogic unit:	A5 i	'm /	LOG OF TEST PIT BU-P-20						
							EST PITS BU-P-1					

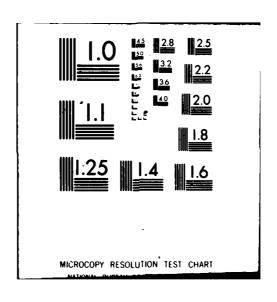
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BULK SAMPLE	ME TERS	PTH	LITHOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION	REMA	RKS	A N/	IEV LYS	318	LL	PI
	0	0		SM		GRAVELLY SAND, brown, fine to coarse, poorly graded, slightly meist, sub- angular, calcareous; some fine to coarse subangular gravel; little silt.							
	- 1	2 -		GP - GM	medium dense	SANDY GRAVEL, light brown, fine, poorly graded, slightly moist, sub-angular, calcareous; some fine to coarse subangular sand; trace silt.		ical stable					
			ATION: 2020' OLOGIC UNIT:		Đm)	TOTAL DEPTH 5.0' (1.5m) LOG OF TEST PIT BU-P-21	,						
	0	1 -				SANDY GRAVEL, light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fina to coarse subangular sand, trace silt.							
1 1	<b>-</b> 1	3 -		GP- GM	medium dense			ical stable					
		4 <del>-</del> 5 <del>-</del>		ec .		SANDY GRAVEL, red brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some fine to coarse subangular sand; little silty clay.  TOTAL DEPTH 5.0' (1.5m)			61	26	13	42	27
URF	NUR I	L GE	ATION: 1810° Dlogic Unit:	( 55)	(M) /A1	LOG OF TEST PIT BU-P-22  LOGS OF TEST VERIFICATION							
						•							

BULK SAMPLE	METERS G		LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS		S JEV		
<b>100</b>	0	O FEET	5		CONS	CILTY CAND Light brown fine to	<b>A</b>	GR	SA	FI	LL P
		1 _				SILTY SAND, light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some silt.					
		2 -		SM	medium dense		vertical walls stable				
	<b>-</b> 1	4 -		SP- SM		SAND, light brown, fine to coarse, poorly graded, dry, subangular, calcareous; race fine subangular gravel; trace silt.	-				
	}	5 -		<b> </b>		TOTAL DEPTH 5.0° (1.5m)	<u> </u>	-			
SURF	ACE	ELEV	ATION: 1870' Ologic Unit:	(570	Om )	LOG OF TEST PIT BU-P-23	1			<u> </u>	
3 UKT	TUIA	L UE	OLUGIC UNIT.	ADY		EUU 01 1E01 111 BU-1-20					
	0	1 -				SAND, brown, fine to coarse, poorly graded, slightly moist, subangular, trace sift; trace fine subangular gravel.		10	78	12	
		3 -		SP- SM	medium dense		vertical walls stable				
	-1	4 -									
	[	5 -				TOTAL DEPTH 5.0' (1.5m)		1		L	ot
<u></u>	ACE I	LEV	ATION: 2030' Ologic unit:	(819 A5v	3m)	LOG OF TEST PIT BU-P-24					
SURF				,		<del></del>		_	_		
SURF SURF							EST PITS BU-P-: ION SITE, BUILE				





BULK SAMPLE	HETERS 30	PTH LEE	LITHOLOGY	nscs	C OMSISTENCY	SOIL DESCRIPTION	REMARKS	S IEV AMALYS GR SA	315	LL	PI
	-1	2 - 3 -		SM	medium dense	SILTY SAND, light brown, fine to coarse, poorly graded, dry, sub- angular, calcareous; some silt.	vertical walls stable				
İ	r	5 -			<u> </u>	TOTAL DEPTH 5.0' (1.5m)	<del></del>	1			
SURF	ACE ICIA	E LEV	ATION: 1240 OLOGIC UNIT:	(37) A50	Bm)	LOG OF TEST PIT BU-P-25					
	0	0						<del>, , , , , , , , , , , , , , , , , , , </del>	Γ-		1
			}								
	ļ	1 -							<u> </u>		
		•						] ] !			
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		2 -	-								
					[						
		_									
	-1	3 -									
			1					}			
		4 -	}								
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	  -	5 -	ļ				· ·	J ) i		,	,
SURF	A CE		1			LOC OF TEST DIT					_
SURF	ACE I		ATION: OLOGIC UNIT:			LOG OF TEST PIT  VERIFICAT	OG OF TEST PIT B	U-P-25	ARI		HA
SURF	ACE I		1			VERIFICAT	TION SITE, BUTLEI	R COP,	ARI		
SURF	ACE ICIA		1			VERIFICAT MX S13	OG OF TEST PIT B TION SITE, BUTLEI TING INVESTIGATION OF THE AIR FOPCE	R COP,	ARI	FI	MA CUI

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SECTION 8.0
SURFICIAL SAMPLE LOGS

#### EXPLANATIONS OF SURFICIAL SAMPLE LOGS

Finalized logs of the surficial samples are presented in this section. The explanations provided here are to serve as general guidelines to reading the logs.

- A. Designations Surficial samples are identified as follows: BU-CS-1
  - BU abbreviation for the site (e.g., BU Butler)
  - CS abbreviation for surficial sample
  - 1 number of activity
- B. Ground Surface Elevation Indicated elevations on the logs are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- C. Surficial Geologic Unit Indicates the surficial geologic unit in which the activity is located.
- D. Depth Indicates depth interval for which soil description is given.
- E. USCS Unified Soil Classification Symbol; see Table 6-1 of Section 6.0, "Boring Logs", for details of USCS.
- F. Soil Description Soil is described based on visual descriptions and/or laboratory test results. See Section 6.0, "Boring Logs", for procedures of soil description.
- G. Sieve Analysis, LL and PI These are from results of laboratory tests. See Section 6.0, "Boring Logs", for explanation.

ACTIVITY	GROUND SURFACE ELEVATION	SURFICIAL Geologic	DE PTH.	uscs	SOIL DESCRIPTION	1 -	IEV ALY:	_		
NUMBER	FEET (METERS)	UNIT	FEET (METERS)			GR	SA	FI	LL	P
BU-CS-2	1985 (605)	A5 i	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, angular, calcareous; some silf					
BU-CS-4	2040 (622)	A5 i	0.0-2.0 (0.0-0.61)	SP-SM	GRAVELLY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, angular; some fine to coarse angular gravel; trace silt.					
BU-CS-6	1770 (539)	A5y	0.0-2.0 (0.0-0.81)	SM	SILTY SAND, brown, fine to medium, poorly graded, medium dense, slightly moist, angular, cal- careous; some silt.	1	68	31		
BU-CS-B	1650 (503)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, angular, calcareous; some silt.					
BU-CS-10	1550 (472)	<b>A5y</b>	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to medium, poorly graded, medium dense, slightly moist, angular, calcareous; some silt.	0	65	35		
BU-CS-12	1530 (466)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to medium, poorly graded, dense, slightly moist, angular, calcareous; little silt					
BU-CS-14	1800 (488)	A5y	0.0-2.0 (0.0-0.61)	CL	SANDY CLAY, light brown, firm, dry, medium plastic, calcareous; some fine to coarse angular sand; trace fine angular to subangular gravel; stage I caliche (0.25'-2.0').					
BU-CS-16	1985 (805)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; little silt; trace fine subrounded gravel.					
8U-CS-18	2115 (845)	A5 i	0.0-2.0 (0.0-0.61)	SM	GRAVELLY SAND, light brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; some fine to coarse subangular gravel; little silt; stage II caliche (1.0'-2.0')			  - 		

LOGS OF SURFICIAL SOIL SAMPLES VERIFICATION SITE, BUTLER CDP, ARIZONA

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ACTIVITY	GROUND SURFACE ELEVATION,	SURFICIAL GEOLOGIC	DE PTH, FEET	uscs	SOIL DESCRIPTION	1 1	ALY:	_		
NUMBER	FEET (METERS)	UNIT	(METERS)			GR	SA	FI	LL	P
BU-CS-20	2210 (874)	A5 i	0.0-1.5 (0.0-0.48)	SH	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular; some silt; trace fine subangular gravel	g	65	26		
			(.5-2.0 (0.46-0.61)	SP-SM	GRAVELLY SAND, light brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, cal— careous; some fine subangular gravel; trace silt					
)U-CS-21	2260 (689)	A5 i	0.0-2.0 (0.0-0.61)	SM	GRAVELLY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; some fine subangular gravel; little silt.					
BU-CS-24	1950 (594)	A5y/A1	0.0-2.0 (0.0-0.61)	SW-SM	GRAYELLY SAND, light brown, fine to coarse, well graded, medium dense, slightly moist, angular, calcareous; some fine to coarse angular gravel; trace silt.	43	52	5		
BU-CS-25	1910 (582)	A5y	0.0-2.0 (0.0-0.61)	GP - GM	SANDY GRAVEL, light brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; some fine to coarse subangular sand; trace silt.					
U-CS-27	1500 (457)	<b>A</b> 5a	0.0-2.0 (0.0-0.61)	GM	SANDY GRAVEL, light brown, fine, poorly graded, medium dense, dry, subangular, calcareous; some fine to coarse subangular sand; little silt					
3U-CS-28	1425 (434)	<b>A</b> 5 i	0.0-2.0 (0.0-0.61)	sc	CLAYEY SAND, light brown, fine to coarse, poorly graded, medium dense, dry, subangular, calcareous; some slightly plastic silty clay.	3	54	43	34	1
3U-CS-30	1360 (415)	<b>A</b> 5 i	0.0-2.0 (0.0-0.61)	SM	GRAVELLY SAND, light brown, fine to coarse, poorly graded, medium dense, dry, subangular, calcareous; some fine to coarse subangular gravel; little silt; stage I caliche throughout.	38	44	18		
BU-CS-37	1810 (552)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to medium, peorly graded, medium dense, slightly moist, subangular, calcareous; some silt.	1	68	31		

LOGS OF SURFICIAL SOIL SAMPLES
VERIFICATION SITE, BUTLER COP, ARIZONA

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ACT IV LTY	GROUND SURFACE ELEVATION	SURFICIAL GEOLOGIC	DE PTH.	uscs	SOIL DESCRIPTION	1	HEV	-		
NUMBER	FEET (METERS)	UNIT	FEET (METERS)	0303	SUIL DESCRIPTION			FI	ıı	P
BU CS-40	1970 (600)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAMD, brown, fine to coarse poorly graded, medium dense, slightly moist, subangular, some sift					
BU-CS-43	1945 (593)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; some silt.	4	66	30		
BU-CS-45	1830 (558)	A5y	0.0-2.0 (0.0-0.61)	ML	SANDY SILT, light brown, firm, slightly moist, slightly plastic, calcareous; some fine to coarse angular sand.					
BU-CS-46	1765 (538)	A5y	0.0-2.0 (0.0-0.61)	ML	SANDY SILT, light brown, firm, slightly moist, nonplastic, caf- careous; some fine to coarse sub- angular sand.					
BU-CS-49	1770 (539)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular,cal-careous; some silt.					
By-CS-51	1810 (552)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAMD, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, calcareous; some silt					
By-CS-52	1820 (555)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, subangular, cal-careous; some silt.					
BU-CS-54	1880 (573)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND; brown, fine to coarse, poorly graded, medium dense, slightly moist, angular, calcareous; some silt					
BU - CS - 56	1510 (460)	A5y	0.0-2.0 (0.0-0.61)	CL	SANDY CLAY, brown, firm, slightly moist, slightly plastic, cal-careous; some fine to medium angular sand	0	49	51	25	1
BU CS:57	1470 (448)	A5y	0.0-2.0 (0.0-0.81)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, angular, calcareous; some silt.					

LOGS OF SURFICIAL SOIL SAMPLES VERIFICATION SITE, BUTLER CDP. ARIZONA

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FIGURE 8-1 3 OF 4

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ACTIVITY	GROUND SURFACE E LEVATION,	SURFICIAL GEOLOGIC	DEPTH,	uscs	SOIL DESCRIPTION		SIEV ALY:	-		
	FEET (METERS)	UNIT	(METERS)			GR	SA	FI	LL	P
BU-CS-59	1470 (448)	A5y	0.0-2 0 (0 0-0 61)	sc	CLAYEY SAND, brown, fine to medium, poorly graded, medium dense, slightly moist, angular, calcareous; some silty clay.	4	62	34		
BU-CS-61	1740 (530)	A5 i	0 0-2.0 (0.0-0.61)	SM	GRAVELLY SAND, light brown, fine to coarse poorly graded, medium dense, slightly moist, angular, calcareous; some fine to coarse angular gravel; little silt; occasional cobbles to 5" size; stage I caliche (1.0'-2.0').	34	50	16		
3U - CS - 83 (	1940 (591)	A5 i	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, light brown, fine to coarse, poorly graded, medium dense, dry, angular, calcareous; some silt; stage I caliche (0.25'- 2.0').					
8U-CS-64	1360 (415)	A5y	0.0-2.0 (0 0-0.61)	SM	SILTY SAND, brown, fine to coarse , poorly graded, medium dense, slightly moist, angular, calcareous; little silt.	2	82	16		
BU - C\$ - 66	1350 (411)	A5y	0.0-2.0 (0.0-0.61)	SM	SILTY SAND, brown, fine to coarse, poorly graded, medium dense, slightly moist, angular to sub-angular, calcareous; little silt; trace fine angular gravel.	5	77	18		

LOGS OF SURFICIAL SOIL SAMPLES VERIFICATION SITE, BUTLER COP, ARIZONA

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FIGURE 8-1

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SECTION 9.0

LABORATORY TEST RESULTS

## EXPLANATIONS OF LABORATORY TEST RESULTS

Laboratory test results are presented in this section. Table 9-1 contains a summary of laboratory test results. This table contains results of sieve analysis; plasticity data; in-situ dry unit weight, moisture content, degree of saturation, and void ratio for drive and Pitcher samples; results of compaction tests; and specific gravity of solids. Other tests such as triaxial compression, unconfined compression, direct shear, consolidation, chemical, and California Bearing Ratio (CBR) are indicated on the table. Tables 9-2 through 9-6 and Figures 9-1 through 9-2 present results of triaxial compression, unconfined compression, direct shear, chemical, and CBR tests.

All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The following table presents the ASTM designations for the tests performed during the investigation.

Type of Test	ASTM	Designations
Particle Size Analysis	D	422-63
Liquid Limit	D	423-66
Plastic Limit	D	424-59
Unit Weight	D	2937-71
Moisture Content	D	2216-71
Compaction	D	1557-70
Specific Gravity of Solids	D	854-58
Triaxial	D	2850-70
Unconfined Compression	D	2166-66
Direct Shear	D	3080-72
Consolidation	D	2435-70
Test for Alkalinity (pH)	D	1067-70
Water Soluble Sodium	D	1428-64
Water Soluble Chloride	D	512-67
Water Soluble Sulphate	D	516-68
Water Soluble Calcium	D	511-72
Calcium Carbonate		1126-67
California Bearing Ratio (CBR)	D	1883-73

Explanation for the tables and figures presented in this section are as follows.

- A. Activity Number Boring, trench, test pit, or surficial sample designation.
- B. Sample Number Prefix indicates the type of sample; explanation is at the bottom of the table.
- C. Sample Interval This is the depth range measured from ground surface over which the sample was obtained.
- D. Percent Finer by Weight Presents the results of laboratory particle size analysis (ASTM D 422-63) performed on representative soil samples at the depth indicated. The numbers represent the percent (by dry weight) of the total sample weight passing through each sieve size indicated.
- E. Atterberg Limits (ASTM D 423-66 and D 424-59)
  - LL Liquid Limit, the water content (as percent of soil dry weight) corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
  - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
  - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
  - NP Nonplastic.
- F. USCS Unified Soil Classification Symbols are given here; see Table 6.1 in Section 6.0, "Boring Logs", for complete details of USCS system.

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- G. In Situ Presents results of tests on drive and Pitcher samples.
  - Dry Unit Weight indicates dry unit weight of soil determined as per ASTM D 2937-71
  - Moisture Content weight of water reported in percent of dry weight of soil sample (ASTM D 2216-71)
  - Saturation the degree of saturation in a soil sample is defined as the ratio (in percent) of the volume of water to the volume of all voids in the soil
  - Void Ratio the numerical ratio of the volume of voids to the volume of solids in a soil specimen
- H. Compacted Indicates results of laboratory maximum dry density and optimum moisture content test as per ASTM D 1557-70.
- I. Specific Gravity of Solids (ASTM D 854-58) Indicates the ratio of (1) the weight in air of a given volume of soil solids at a stated temperature, to (2) the weight in air of an equal volume of distilled water at a stated temperature.
- J. Triaxial The triaxial compression tests were performed in accordance with the procedures of ASTM D 2850-70. The following explanations and definitions apply.

Triaxial Compression Test - a cylindrical specimen of soil is surrounded by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied, directed along the axis of the specimen called the axial load.

Consolidated-Drained (CD) Test - a triaxial compression test in which the soil was first consolidated under an all-around confining stress (test chamber pressure), and was then compressed (and hence sheared) by increasing the vertical stress. Drained indicates that excess pore water pressure generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-Undrained (CU) Test - a triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear test at constant water content.

Confining Pressure ( $\sigma_3$ ) - the isotropic chamber pressure applied to the soil specimen during consolidation and compression.

Maximum Deviator Stress  $(\sigma_1-\sigma_3)$  - the difference between the major and minor principal stresses in the specimen at failure. The major principal stress on the specimen is equal to the unit axial load plus the chamber pressure and the minor principal stress on the specimen is equal to the chamber pressure.

Strain Rate — axial strain,  $\epsilon$ , at a given stress level is defined as the ratio of the change in length  $(\Delta L)$  of the specimen to the original length of the specimen  $(L_0)$ . The rate of strain was controlled during the test so that this ratio increased at equal increments for each minute of testing.

Back Pressure - pressure in excess of atmospheric applied to the pore water of a soil sample. Back pressure is usually applied to (1) increase saturation of the sample, or (2) simulate the actual in-situ pressure regime.

- K. Unconfined Compression Test procedures were as described in ASTM D 2166-66. Unconfined compressive strength is defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test. In these methods, unconfined compressive strength is taken as the maximum load attained per unit area or the load per unit area at 20 percent axial strain, whichever occurred first during the performance of a test.
- L. Direct Shear The procedures of ASTM D 3080-72 were followed for direct shear testing. In this test, soil under an applied normal load is stressed to failure by moving one section of the soil container (shear box) relative to the

other section. Normal stress is the value of load per unit area acting perpendicular to the plane of shearing. Maximum shear strength is defined as the maximum resistance (ksf) of a soil to shearing (tangential) stresses.

- M. Consolidation (ASTM D 2435-70) A consolidation test is a test in which a cylindrical soil specimen is laterally confined in a ring and compressed between porous plates. The term "consolidation", as used here, indicates the gradual reduction in volume of the soil mass resulting from an increase in compressive stress (axial load per unit area).
- N. Chemical The chemical tests performed on soil samples included: pH; water soluble sodium, chloride, sulphate, calcium; and calcium carbonate content. pH is an index of the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

  ASTM test procedure designations for these chemical tests are included in the table at the beginning of the "Explanation of Laboratory Test Results".
- O. CBR California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a standard crushed-rock base material. The procedures for conducting a CBR test were as outlined in ASTM D 1883-73. The materials tested for CBR were also analyzed for particle size distribution (ASTM D 422-63) and compaction characteristics (ASTM D 1557-70). The term "percentage of maximum density" indicates the ratio (as a percentage) of the compacted sample

dry unit weight to maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture-Density Relations of Soils Using 10-pound (4.5 kg) Hammer and 18-inch (457 mm) Drop."

				Γ					PERCE	IT FINE	R BY V	VE I GHT	
=	(a)	SAMPLE I	NTFRVAL		2.	TANDARD	SIEV					STAN	DARD
ACT I V I TY Number	SAMPLE NUMBER	SAMILL I	MI ENTAL	BLDRS.	COBE	LES		GRA	VEL			SA	
₩ ₩	SA	FEET	METERS	24"	12"	6"	3"	1½"	3/4"	3/8"	4	10	40
BU-B-1	P-1	1.0-3.7	0.30-1.13										
	P-2	4.0-6.5	1.22-1.98							100	99	89	21
	D-3	7.0-8.0	2.13-2.44										
	D-4	10.2-10.9	3.11-3.32						100	97	92	81	43
	<b>D-5</b>	15.0-15.7	4.57-4.79										
	D∺6	20.2-20.9	6.16-6.37						100	97	94	69	35
	D-7	25.0-26.0	7.62-7.92										
	D-8	30.2-30.7	9.20-9.36						100	97	91	76	34
	D-9	40.0-41.0	12.19-12.50										
	D-10	50.0-51.0	15.24-15.54							100	98	78	17
	D-11	60.0-61.0	18.29-18.59										
	D-12	68.0-69.0	20.73-21.03						_				
	D-13	80.4-80.9	24.51-24.66							100	96	73	25
	D-14	90.0-91.0	27.43-27.74										
	D-15	100.2-100.9	30.54-30.75							100	94	66	2 <b>2</b>
	D-16	107.2-107.9	32.67-32.89							100	99	98	77
	D-17	116.0-117.0	35.36-35.66										
	D-18	129.4-129.9	39.44-38.68							100	93	73	26
	D-19	145.0-146.0	44.20-44.50										
	D-20	160.4-160.9	48.89-49.04						100	94	91	77	26
BU-B-2	P-1	0.0-2.7	0.00-0.82	L]									
	r-2	3.5-4.3	1.07-1.31					100	96	90	85	71	21
	D-3	6.0-7.0	1.83-2.13	$L^{-1}$									
	D-4	10.2-10.9	3.11-3.32										
	D-5	15.2-15.9	4.63-4.85						100	99	97	91	60
	D-6	20.0-21.0	6.10-6.40										
	D-7	25.0~25.6	7.62-7.80								100	99	98
	P-8	30.0-31.1	9.14-9.48									100	99
	D-9	37.1-37.7	11.31-11.49						100	92	73	53	2 <b>2</b>
	D-10	41.2-41.9	12.56-12,77								100	93	74
	P-12	58.0-59.3	17.68-18.07	lacksquare						100	98	89	52
<b></b>	D-13	71.0-72.0	21.64-21.95						L				
	D-14		24,38-24.69										
	0-15		27.49-27.71						100	95	87	56	15
	D-16		29.87-30.11										
		108.5-110.5	33.07-33.68										
		120.7-121.4										100	95
		130.0-131.7											
	P-20		43.89-44.17								100	99	93
	P-21	160.0-161.9	48.77-49.35						100	96	94	90	70
BU-B-3	D-1	0,0-1.0	0.00-0.30										

## NOTES:

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
- P Pitcher
- (d) \* Indicates that test has been performed and results are included in this report
- D Fugro Orive
- B,b Bulk
- (b) NP Not Plastic

SILT OR CLAY															040.07-					
SM   107.4   1720   5.4   25.6   0.57   2.64			NIA-	1016	47	TEDDE	DC			- 11	1-5110			<u>C</u>	UMPACIE		ام	€		
SM   107.4   1720   5.4   25.6   0.57   2.64	E NO	<b>)</b>						uscs			S F	TION				E E		KIAL	UNCONFINED COMPRESSION	5
SM	T	SIL	T OR C	LAY			`-'		WEIG	SHT	2 H 2	<b>E S</b>		DRY DE	MSITY	E 2 2	S ₹ EC	IA		DIRECT
SM   107.4   1720   5.4   25.6   0.57   2.64	0	200	.005	.001	LL	PL	PI	(1)	(pcf)	(kg/m <sup>3</sup> )		SAT	YO.	(pcf)	$(kg/m^3)$	8 =	282	=	38	5
SP   107.9   1728   1.2   6.0   0.53   2.64	+			_				SM			5.4	25.6			*					
SP   112,1   1796   1.0   5,4   0,50	1	7	<del></del>		<b> </b>	<b>-</b>	<del> </del>									<del>                                     </del>	2.64			
33   29	$\dashv$	-			-															•
SM   108.4   1736   14.3   69.7   0.55	3	29		<u> </u>	74	28	46									1		· "		
SM	+						<del>                                     </del>													
SP-SM   111.4   1784   6.9   36.4   0.51	<u> </u>	17					<u> </u>												L	
17   12   SW-SM   113.1   1812   5.6   30.9   0.49	十										6.9									-
SP-SM   116.2   1861   7.6   45.6   0.45	7	12		Ī ———				SW-SM	113.1	1812	5.6								L	
SP-SM   SP-SM   SP-SM   SP-SM   SP-SM   109,4   1752   4.5   2.3,2   0.42	$\neg$		Ī				T													
SP-SM   109.4   1752   4.5   22.5   0.54	一	5	Ī																	
SP-SM   118.4   1897   5.2   33.2   0.42	丁		Γ					SP-SM	109.4		4.5									وا
SP-SM   113.9   1825   4.2   23.7   0.48								SP-SM	118.4	1897	5.2	33.2	0.42				ļ		<b> </b>	<b>↓</b>
12   10   SW-SM   119.2   1909   5.6   36.6   0.41	3	11						SP-SM	118.1	1892	5.2					<u> </u>	<u> </u>	L	<b> </b>	11
SM								SP-SM	113.9	1825	4.2	23.7	0.48			<u> </u>		L	<b>_</b>	$\vdash$
SM   113.0   1810   8.7   47.8   0.49	2	10						SW-SM	119.2	1909	5.6					<u> </u>	ļ	L	<b></b>	<b>↓</b> ⊸
SW-SM   121.7   1949   3.2   22.5   0.38	2	32					$\Box$	SM	114.8							L	<u> </u>	<u> </u>	ļ	1
SW-SM   122.4   1961   5.1   36.6   0.38	$\perp \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \!$		L	L					113.0								ļ		<b> </b>	1-4
SW-SM   120.7   1933   4.4   30.0   0.40	1	8			<u> </u>		L	SW-SM	121.7						<u> </u>	<b>ļ</b>	<b>}</b>	<b>ļ</b>	↓	1
SP-SM   80.6   1291   16.8   41.6   1.09			L				<u> </u>				•				<u> </u>	↓	<b></b> _	<b> </b>	<b>├</b> ──	╀┪
10   8   SW-SM   1.8	2	9		<b></b>			L_	SW-SM	120.7	1933	4.4	30.0	0.40	ļ		<u> </u>	<b>↓</b>	<b>!</b>	<del> </del>	1-4
10   8   SW-SM   1.8   SP-SM   115.6   1852   2.5   14.8   0.46   SM   109.8   1759   4.5   23.6   0.51   2.65			l	Ĺ	L	L				ļ					<u> </u>	<u> </u>	<del> </del>		∔	╂╌┩
SP-SM   115.6   1852   2.5   14.8   0.46	$\perp$		L	L	L		L	SP-SM	80.6	1291		41.6	1.09			<b>_</b>	<b></b> _	<b> </b>	<b>↓</b>	╂╼┩
SM       109.8       1759       4.5       23.6       0.51       2.65         37       30       SM       113.5       1818       5.0       27.9       0.48       0.68         ML       98.4       1576       10.6       40.2       0.71       0.68       0.69       0.68       0.68       0.68       0.69       0.68       0.68       0.68       0.69       0.68       0.68       0.68       0.69       0.68       0.68       0.69       0.68       0.68       0.68       0.68       0.69       0.68       0.68       0.68       0.69       0.68       0.68       0.68       0.69       0.68       0.68       0.69       0.68       0.68       0.69       0.68       0.69       0.68       0.69       0.68       0.69       0.69       0.68       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69       0.69 <td><u> </u></td> <td>8</td> <td></td> <td></td> <td><u> </u></td> <td></td> <td>L_</td> <td></td> <td></td> <td><u> </u></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td><u> </u></td> <td><b></b></td> <td><b></b></td> <td><b>↓</b></td> <td>╁╼┩</td>	<u> </u>	8			<u> </u>		L_			<u> </u>						<u> </u>	<b></b>	<b></b>	<b>↓</b>	╁╼┩
SM   113.5   1818   5.0   27.9   0.48	ᆚ			L										<u> </u>	L	-	<del> </del>	<b>-</b>	<b>∔</b> -	╂╼┪
ML       98.4       1576       10.6       40.2       0.71         92       80       ML       100.0       1602       10.7       42.2       0.68         94       87       ML       93.0       1490       16.5       54.9       0.81         8       5       SP-SM       121.1       1940       4.9       33.8       0.39         54       42       SM       121.5       1946       3.9       27.2       0.39         37       31       SM       105.9       1696       9.5       43.4       0.59         5P       104.0       1666       6.3       27.4       0.62         SP       116.4       1865       3.3       19.9       0.45         7       4       SW       122.9       1969       7.5       54.6       0.37         SM       101.2       1621       14.7       59.7       0.66         SM       99.7       1597       21.8       85.3       0.69					<u> </u>		<u> </u>							Ļ		<del>  </del>	2.65	<b>├</b> ──	┼	<b>↓_</b> ¶
92       80       ML       100.0       1602       10.7       42.2       0.68         94       87       ML       93.0       1490       16.5       54.9       0.81         8       5       SP-SM       121.1       1940       4.9       33.8       0.39         54       42       SM       121.5       1946       3.9       27.2       0.39         37       31       SM       105.9       1696       9.5       43.4       0.59         SP       104.0       1666       6.3       27.4       0.62         SP       116.4       1865       3.3       19.9       0.45         7       4       SW       122.9       1969       7.5       54.6       0.37         SM       101.2       1621       14.7       59.7       0.66         SM       99.7       1597       21.8       85.3       0.69	7	30		L	<u> </u>	<u> </u>								<u> </u>		<b>↓</b>	<b>↓</b>	<b>├</b> ─	+	╁╼┩
94       87       ML       93.0       1490       16.5       54.9       0.81         8       5       SP-SM       121.1       1940       4.9       33,8       0.39         54       42       SM       121.5       1946       3.9       27.2       0.39         37       31       SM       105.9       1696       9.5       43.4       0.59         SP       104.0       1666       6.3       27.4       0.62         SP       116.4       1865       3.3       19.9       0.45         7       4       SW       122.9       1969       7.5       54.6       0.37         SM       101.2       1621       14.7       59.7       0.66         SM       99.7       1597       21.8       85.3       0.69			<u> </u>	<u> </u>		<u> </u>	<b>↓</b> _				<del></del>			<u> </u>	<del></del>	<del> </del> _	<b>├</b> ──	<b>}</b> —-	<del> </del>	+
8       5       SP-SM       121.1       1940       4.9       33,8 0.39         54       42       SM       121.5       1946       3.9       27.2 0.39         37       31       SM       105.9       1696       9.5       43,4 0.59         SP       104.0       1666       6.3       27.4 0.62         SP       116.4       1865       3.3       19.9 0.45         7       4       SW       122.9       1969       7.5       54.6 0.37         SM       101.2       1621       14.7       59.7 0.66         SM       99.7       1597       21.8       85.3 0.69	$\overline{}$		—		<u> </u>	<u> </u>	↓							<b></b>	<del> </del> -	<del> </del> _	<del>                                     </del>	<del> -</del> -	+	╂╼┪
54     42     SM     121.5     1946     3.9     27.2     0.39       37     31     SM     105.9     1696     9.5     43.4     0.59       SP     104.0     1666     6.3     27.4     0.62       SP     116.4     1865     3.3     19.9     0.45       7     4     SW     122.9     1969     7.5     54.6     0.37       SM     101.2     1621     14.7     59.7     0.66       SM     99.7     1597     21.8     85.3     0.69			L	L	<u> </u>	<u> </u>									L	<del></del>	<del> </del> -	<del> </del>	<del> </del>	+-4
SM   105.9   1696   9.5   43.4   0.59					L	<u> </u>	<b> </b>							<u> </u>	<del> </del>	<b>├</b>		<b>↓</b> —	+	╂╼┩
SP     104.0     1666     6.3     27.4     0.62       SP     116.4     1865     3.3     19.9     0.45       7     4     SW     122.9     1969     7.5     54.6     0.37       SM     101.2     1621     14.7     59.7     0.66       SM     99.7     1597     21.8     85.3     0.69			<u> </u>	<u> </u>	<u> </u>	<u> </u>	L							<b> </b>	<b>├</b>	<del> </del>	<del> </del>	<del> </del>	+	+-4
SP 116.4 1865 3.3 19.9 0.45  7 4 SW 122.9 1969 7.5 54.6 0.37  SM 101.2 1621 14.7 59.7 0.66  SM 99.7 1597 21.8 85.3 0.69	7	31	<b>├</b>	ļ <u>.</u>	<b> </b>	ļ	<b> </b>								<b>├</b>	<del> </del>	<del> </del>	<del> </del>	+	1-4
7 4 SW 122.9 1969 7.5 54.6 0.37 SM 101.2 1621 14.7 59.7 0.66 SM 99.7 1597 21.8 85,3 0.69	$\dashv$		-	<u> </u>	<b>├</b> ──	-									<del> </del>	<del> </del>	<del> </del>	<del> </del>	╅	1-1
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SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION

EPARTMENT OF THE AIR FORCE - SAMSO

7ABLE 8-1 1 07 4

IGRO NATIONAL INC.

47.5-48.5	14.48-14.78	I I
60,0-60.5	18.29-18.50	
88.2-88.9	26,88-27.10	
99.0-99,5	30,18-30,33	
110.0-110.5	33.53-33.68	
120.0-120.5	36.58-36.73	
130.0-130.4	39.62-39.75	
144.0-144.3	43.89-43.98	
0.0-2.8	0.00-0.85	
3.7-4.4	1.13-1.34	
6.0-7.0	1.83-2.13	
10.2-10.9	3.11-3.32	
15.2-15.9	4.63-4.85	
19.0-20.0	5.79-6.10	
25.0-25.6	7.62-7.80	
30.0-30.7	9.14-9.36	
40.0-41.0	12.19-12.50	
50.0-50.7	15.24-15.45	
60.1-60.8	18.32-18.53	
70.0-70.8	21.34-21.58	
80.0-80.6	24.38-24.57	
90.2-90.9	27.49-27.71	
100.0-101.0	30.48-30.78	

[		l	SP-SM	109.8	1759	6.2	31.3
			SW-SM	124.6	1996	5,8	44.5
37	19	18	SC	106.7	1709	10.4	48.5
			SP-SM	121.3	1943	3.6	25.0
			SM	107.5	1722	8.6	40.9
			SW-SM	127.2	2038	6.7	55.7
			SP-SM	125.3	2007	6.0	47.0
			SP-SM	123.8	1983	7.3	54,6
			SW-SM	132,7	2126	5.8	58.1
			SW-SM	137.0	2195	4.9	57.6
			SW-SM	136.4	2185	5.3	60.8
			SM				
			SM	104.2	1669	5.5	24.1
			SM	106.7	1709	3.9	18.2
			SM	114.2	1829	5.4	30.7
			SM	109.3	1751	5.2	27.3
			SW-SM	121.2	1941	5.8	41.3
			SM	122.4	1961	5.2	37.3
46	20	26	SC	116.4	1865	7.6	45.9
			SM	117.4	1881	8.8	54.6
			SM	111.2	1781	7.0	36.7
			SM	112.0	1794	7.7	41.2
			SM	110.1	1764	9.8	49.9
			SM	96.8	1550	8.3	30.3
			SM	117.4	1881	13.3	82.5
			SM	120.3	1927	6.6	44.5
			SM	122.2	1957	5,8	41.3
			SM	122.1	1956	8.3	59.0

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	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	1	CONSOLIBATION	_ ا	
		EAX	CONF.	DIRECT	20110	CHEMICAL	_
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SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE, BUTLER COP, ARIZONA

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AC E	S Z	FEET	METERS	24"	12"	6"	3"
BU-B-5	D-7	25.2-25.9	7.68-7.89				
	D-8	29.1-29.6	8.87-9.02				
	D-9	35.0-35.6	10.67-10.85				
	P-10	40.0-41.6	12.19-12.68				
	D-11	50.0-50.7	15,24-15,45				
	D-12	60.0-60.4	18,29-18,41				
	D-13	70.0-70.4	21.34-21.46				
	D-14	81.0-81.6	24.69-24.87				
	D-15	90.0-90.6	27.43-27.62				
	D-16	100.0-100.4	30.48-30.60				
	D-17	110.0-110.4	33.53-33.65				
	D-18	120.0-120.4	36.58-36.70				
	D-19	130.2-130.9	39.68-39.90				
	D-20	145.0-145.4	44.20-44.32				
	D-21	160.5-161.4	48.92-49.19				
BU-T-1	B-1	0.5-2.0	0.15-0.61				
	b-2	3.5-4.0	1.07-1.22				
BU-T-2	B-1	0.5-2.0	0.15-0.61				
BU-T-3	B-1	0.5-2.0	0.15-0.61				
	b-2	7.0-8.0	2.13-2.44				
BU-T-4	B-1	0.5-2.0	0.15-0.61				
	b-3	8.0-9.0	2.44-2.74				
BU-T-5	B-1	0.5-2.0	0.15-0.61				
	b-2	3.0-4.0	0.91-1.22				
BU-P-3	B-2	2.0-3.0	0.61-0.91				

	TERBE		USCS (c)	DRY U		MOISTURE Content (%)	SATURATION (\$)	VOID RATIO	MAXI Dry de	MUM NSITY	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL	MI SHOOME
IL	PL	PI		(pcf)	(kg/m³)	물음	SAT	YO RA	(pcf)	(kg/m³)	5 ¥	2 2 2	Ξ.	
			SW-SM	122.7	1965	4.0	28.9	0.37						, and
			SM	106.4	1704	9.9	45.8	0.58						
			SM	102.4	1640	11.3	47.3							
			SM	109.5	1754	10.4	52.1	0.54						-
			SM	126.8	2031	5.5	45.2				<del></del>			-
			SP-SM	127.3	2039	7.6	63.4	0.32				<b>├</b>		H
		-	SM	130.3	2087	6.5	59.9	0.29						-
		$\vdash$	SM	128.3 118.0	2055	4.6	39.7		. <u></u> .					
			SM SM	123.6	1890	9.0 7.4	56.8							j
-		$\vdash$	SM	131.3	1980 2103	6.1	55.0 58.2			<u> </u>				H
		-	SP-SM	134.7	2158	6.3	67.8	0.25				1		1
			SP-SM	131.6	2108	4.3		0.28						
			SM	134.9	2161	5.2	56.4	0.25						
			SM	134.6	2156	4.5	48.3							
			SM				·							
30	14	16	SC											
			SM						136.7	2190	6.8		L	
											<u> </u>	<b>_</b>		
			SP-SM			L		ļ			<u> </u>			1
		·NP	SW-SM					L						14
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		$\Box$	SM						123.0	1970	10.9			
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			SM			<del>                                     </del>	<del>-</del> -	-	<b></b>		<del> </del>			
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27	17	10	SC											
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21	18	3	ML		<u> </u>	ļ	<b></b>	<u> </u>	125.5	2010	9.1			1-1
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PACTE	0		9	_ Z		善		
SITY (kg/m³)	OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHEMICAL	C8.R
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2190	6.8							•
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SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE, BUTLER COP. ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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<b>E</b>	(8)	SAMPLE I	MTERVAL		2	TANDARI	SIEV	E OPEN			U S		ID A RA
ACTIVITY Number	SAMPLE NUMBER	)	** * *** * ***	BLDRS.	COBE	BLES	Γ	GRA	VEL			SA	ND
AC NO.	SA	FEET	METERS	24"	12"	6"	3"	14"	3/4"	3/8"	4	10	40
BU-P-16	B-1	0.25-1.5	0.08-0.46				100	93	82	65	53	42	29
BU-P-17	b-1	0.5-2.0	0.15-0.61							100	98	93	6 <b>5</b>
BU-P-18	B-1	0.5-2.0	0.15-0.61	<b></b>				100	90	83	76	63	36
BU-P-20	B-1	0.5-2.0	0.15-0.61				100	91	71	62	55	46	31
BU-P-22	B-2	4.0-5.0	1.22-1.52					100	74	57	39	28	14
BU-P-24	b-1	0.5-2.0	0.15-0.61						100	97	90	69	21
BU-CS-6	b-1	0.5-2.0	0.15-0.61							100	99	96	7
BU-CS-10	B-1	0.5-2.0	0.15-0.61	1							100	99	86
BU-CS-20	b-1	0.5-1.5	0.15-0.46			<u> </u>			100	95	91	84	67
BU-CS-24	B-1	0.5-2.0	0.15-0.61					100	96	81	57	32	12
BU-CS-28	b-1	0.5-2.0	0.15-0.61	1		<b></b>	<u> </u>	ļ	100	99	97	89	67
BU-CS-30	b-1	0.5-2.0	0.15-0.61					100	81	70	62	50	28
BU-CS-37	b-1	0.5-2.0	0.15-0.61							100	99	92	55
BU-CS-43	b-1	0.5-2.0	0.15-0.61			<u> </u>			100	99	96	86	3
BU-CS-56	B-1	0.25-2.0	0.08-0.61									100	86
BU-CS-59	B-1	0.5-2.0	0.15-0.61				<u> </u>	ļ	100	98	96	92	71
BU-CS-61	B-1	0.25-2.0	0.08-0.61					100	83	74	66	55	31
BU-CS-64	B-1	0.25~2.0	0.08-0.61							100	98	92	55
BU-CS-66	B-1	0.5-2.0	0.15-0.61	<b> </b>	⊢ ├	<u> </u>			100	99	95	79	4
			<del> </del>	<b> </b>									

## NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

\$\$ - Standard split spoom

- P Pitcher
- (d) \* Indicates that test has been performed and results are included in this report
- 0 Fugro Orive B,b - Bulk

(b) NP - Not Plastic

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		S	I SIZ	E (mm)	الم	IMITS	(b)	USCS (c)	DRY Wei	unit Sht	MOISTURE CONTENT (%)	SATURATION (\$)	_=	MAXI Dry De	MUM :NS 1 TY	OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT
<b>32</b>	100	$\rightarrow$	.00	5 .001	LL	PL	PI	<b>1</b> ``´	(pcf)	(kg/m³)	들증	SATU	VOID RATIO	(pc1)	(kg/m³)		SPE GRA OF	₹	3 5	=
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	14	13	<b>1</b> —	+-	42	15	27	GC						124.0	22.45				ļ	-4
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SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE. BUTLER COP. ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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UGRO NATIONAL ING.

BORING	SAMPLE	SAMPLE	INTERVAL	SOIL	NORMAL	STRESS		IMUM Strength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m²
BU-B-1	D-3	7.0-8.0	2.13-2.44	SP	1.0	48	1.4	68
					2.0	96	1.9	90
					3.0	144	3.1	150
8U-B-1	D-7	25.0-26.0	7 . 62 - 7 . 92	SP-SM	2.5	120	2.5	122
					5.0	239	4.6	221
					7.5	359	8.2	391
BU-B-1	D-11	60.0-61.0	18.29-18.59	SP-SM	6.0	287	5.8	277
					8.0	383	7.4	354
					12.0	575	9.5	457
BU-B-2	D-4	10.2-10.9	3.11-3.32	MZ	1.0	48	1.7	80
					2.0	96	2.7	129
					3.0	144	3.1	149
BU-B-2	P-8	30.0-31.1	9.14-9.48	ML	3.0	144	2.6	126
					6.0	287	4.8	232
					9.0	431	7.8	375
BU-B-3	D-10	40.1-40.8	12.22-12.44	SP-SM	4.0	192	4.2	200
					8.0	383	7.3	350
					12.0	575	10.8	516
BU-B-4	D-4	10.2-10.9	3.11-3.32	SM	1.0	48	2.2	103
					2.0	96	2.9	138
BU - B - 4	0-5	15.2-15.9	4.83-4.85	SP-SM	1.5	12	2.0	95
					4.5	215	4.2	199
BU-B-5	D-9	35.0-35.6	10.67-10.85	SM	3.0	144	6.5	312
					6.0	287	9.1	434
					9.0	431	11.3	542

SUMMARY OF DIRECT SHEAR TEST RESULTS VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

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UGRO NATIONAL INC.

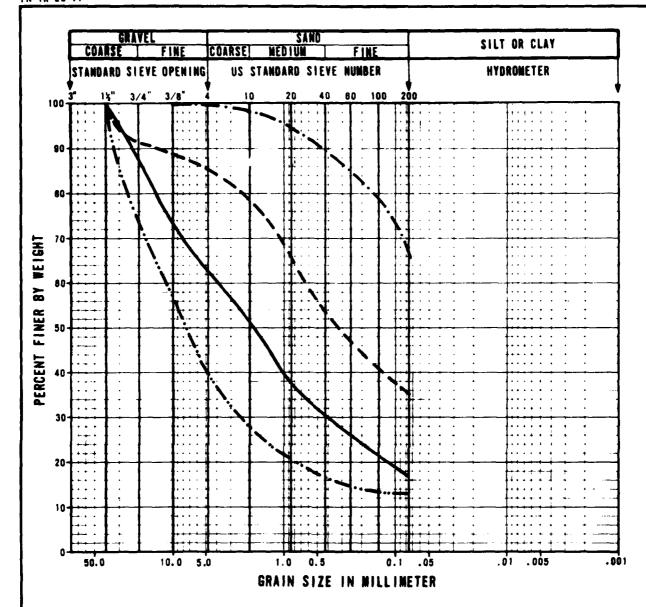
1		CAMBIE INTERVE					3	NATER SOLUBLE	in in	CALCIUM
ACTIVITY	SAPLE		MICHARL	SOIL	푎	MA 1 00 S	CHLORIDE	SULPHATE	CALCIUM	CARBONA TE
		FEET	METERS			mg/kg	mg/kg	mg kg	<b>高</b> 大名	ag 'kg
BU-8-2	<b>p</b> -1	0.0-2.7	0.00-0.82	SP-SM	7.5	22	25	11	9,6	272
	0-6	20.0-21.0	6.10-6.40	ML	7.4	116	959	172	456	1798
	P-12	58.0-59.3	17.68-18.07	SM	7.5	001	118	413	94	158
	0-16	98.0-98.8	29.87-30.11	NS	7.6	49	15	693	11	95
	P-20	144.0-144.9	43.89-44.17	CL	7.5	72	17	24	24	96
BU-8-4	P-1	0.0-2.8	0.00-0.85	NS	6.1	26	15	643	98	251
	D-6	19.0-20.0	5.79-6.10	SM	6.5	331	295	230	29	147
	0-12	70.0-70.8	21.34-21.58	NS.	8.8	246	286	545	16	53
	0-16	110.0-110.9	33.53-33.80	NS.	<b>9.4</b>	342	295	849	573	1939
BU-T-4	8-1	0.5-2.0	0.15-0.61	SM	6.5	39	10	212	39	140
BU-T-5	8-1	0.5-2.0	0.15-0.61	SM	6.0	91	22	1495	57	- 188 - 188
BU-P-13	8-1	0.25-2.0	0.08-0.61	ML	6.1	32	15	16	7.0	338
BU-CS-61	8-1	0.25-2.0	0.08-0.61	SM	6.1	16	15	53	63	184
		÷								

SUMMARY OF CHEMICAL TEST RESULTS VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

1 A B L E

UBRO MATIONAL INC



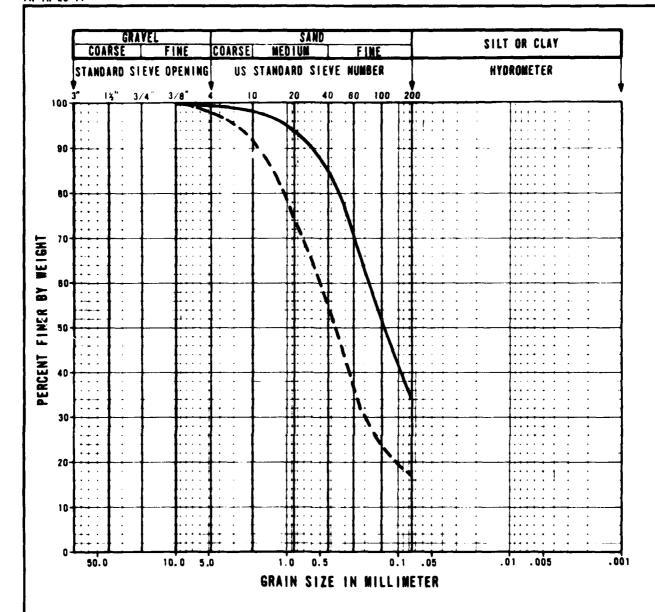
SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
SIMPUL	NUMBER	NUMBER	FEET	METERS	TYPE
	A	BU-T-2	0.5-2.0	0.15-0.61	M2
	В	BU-T-4	0.5-2.0	0.15-0.61	- SM
	C	BU-P-13	0.25-2.0	0.08-0.61	ML
	D	BU-P-22	4.0-5.0	1.22-1.52	GC

GRAIN SIZE CURVES, CBR TESTS
VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

9-1

MORO MATIONAL INC.



SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
21MDAL	NUMBER	NUMBER	FEET	METERS	TYPE
	E	BU -CS -10	0.5-2.0	0.15-0.61	MZ
	F	BU-CS-84	0.25-2.0	0.08-0.61	SM
		F			$\{ - \}$
					T

GRAIN SIZE CURVES, CBR TESTS VERIFICATION SITE, BUTLER CDP. ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

9-1 2 0F 2

MORO MATIONAL INC

COMPOSITE	SOIL	PERCENT	ATTEI	ATTERBERG LIMITS	SPECIFIC	MAXIMUM DRY DENSITY	I MUM INSITY	OPT IMUM Moisture	COMPACTED DRY DENSITY	CTED	COMPACTED	PERCENT OF	CBR
KUMBER	ITPE	#200	11	l d	GRAVITY	pc f	kg/m3	(S)	pcf	kg/m3	<b>%</b>	ORY DENSITY	<u>\$</u>
									132.3	2119	6.1	8 . 36	06
									125.8	2015	7.4	92.0	45
~	NS.	11				136.7	2190	8.9					
									122.6	1964	11.7	9.66	43
									117.9	1889	11.4	82.8	33
<b>~</b>	S	34				123.0	1970	10.9	108.3	1735	11.7	0.88	6
									125.1	2004	9.1	99.7	81
									118.3	1895	9.3	94.3	28
ບ	Ħ	99	12	ო		125.5	2010	9.1	110.6	1772	9.3	1.88	€
									133.8	2143	6.5	99.9	50
									127.8	2047	6.3	95.4	41
6	39	5	42	27		134.0	2146	7.2	121.1	1940	6.7	90.4	11

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-4

**VORO NATIONAL INC** 

AFV-13

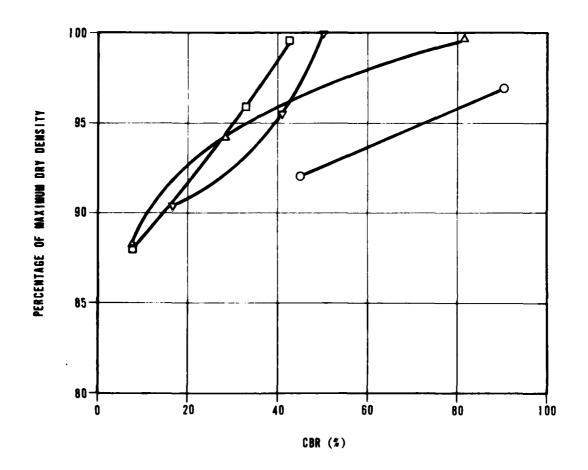
40 40	14 98
100.0 84.3 91.7	94.3 91.7
7.6	7.6
1901	1849
116.7	116.7
7.4	7.4
2017	
125.9	125.9
91	91
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u.	<b>L</b>

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS VERIFICATION SITE, BUTLER CDP. ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-4 2 OF 2

VERO NATIONAL INC.



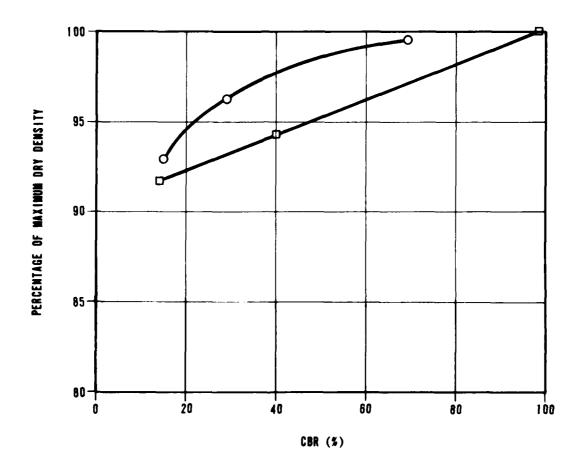
SYMBOL	COMPOSITE Sample Number	SOIL
0	A	SM
	В	SM
Δ	C	ML
▽	0	GC

CALIFORNIA BEARING RATIO (CBR) CURVES VERIFICATION SITE, BUTLER CDP, ARIZONA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

9-2 1 0f 2

**VERO NATIONAL INC** 



SYMBOL	COMPOSITE SAMPLE NUMBER	SOIL TYPE
0	Ε	SM
	F	SM

CALIFORNIA BEARING RATIO (CBR) CURVES VERIFICATION SITE, BUTLER CDP, ARIZONA

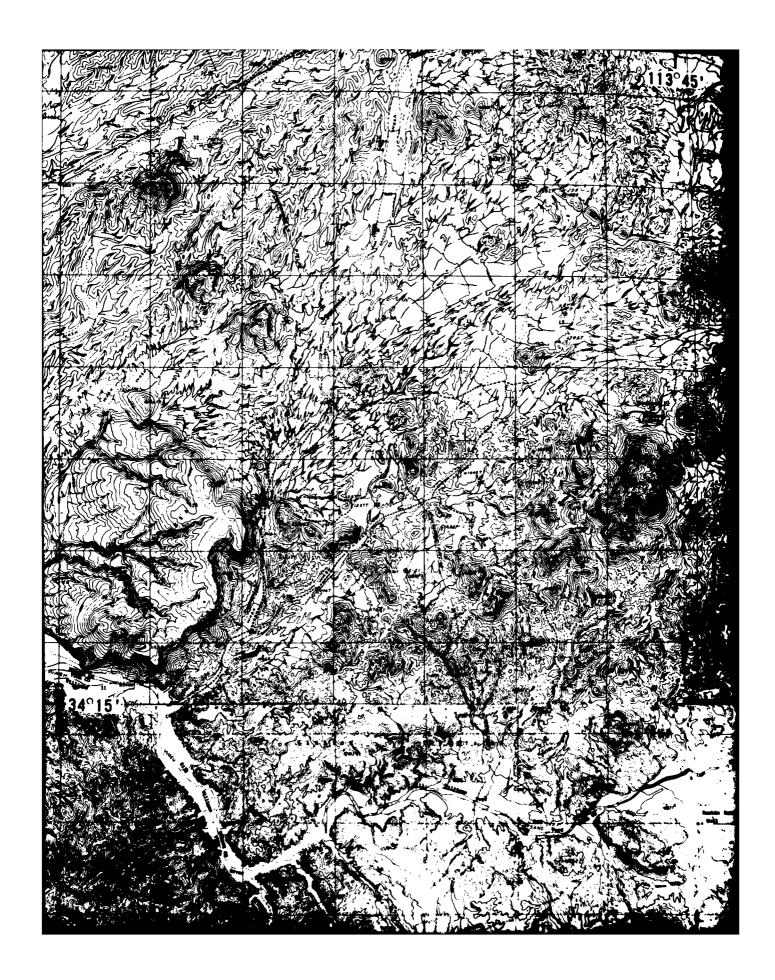
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

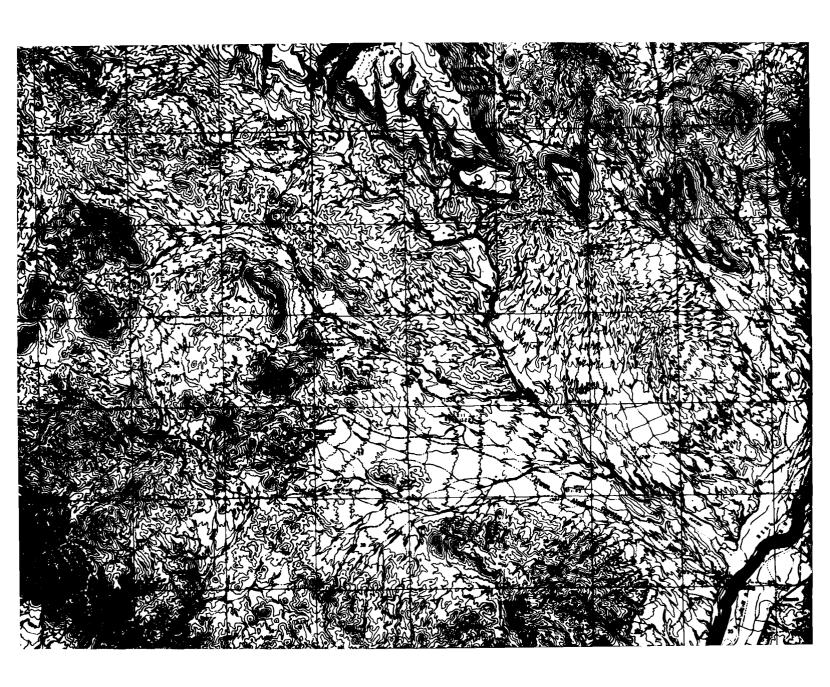
9-2 2 0F 2

UBRO NATIONAL INC

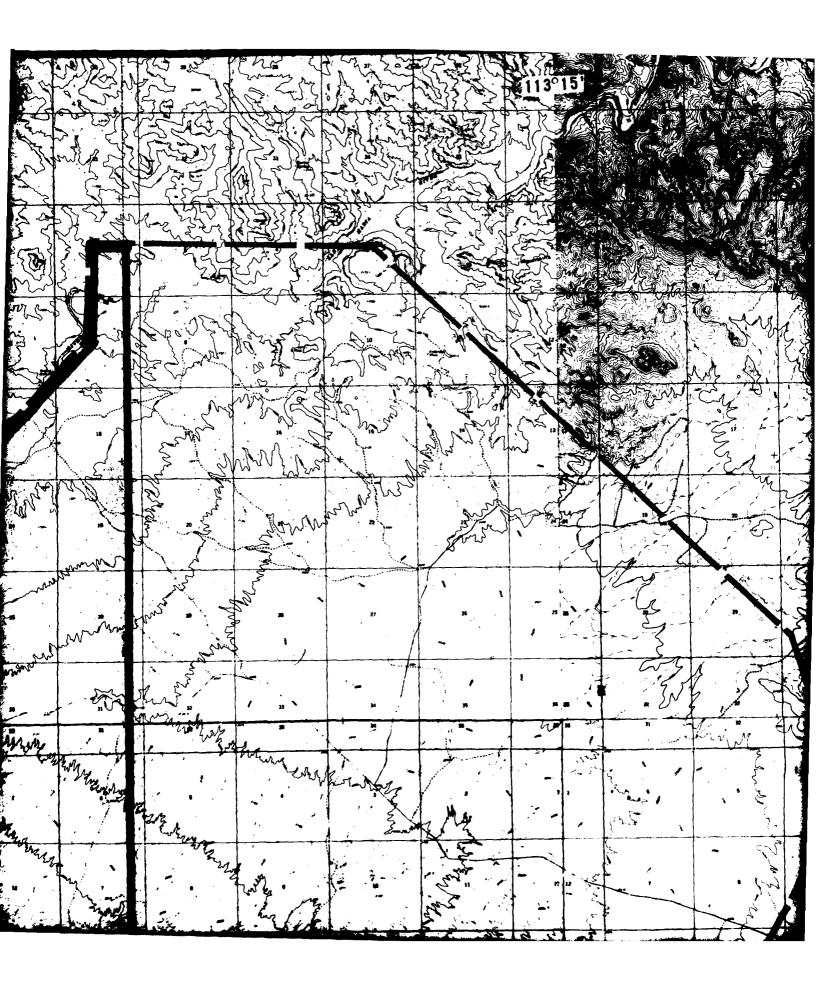
AFV-14

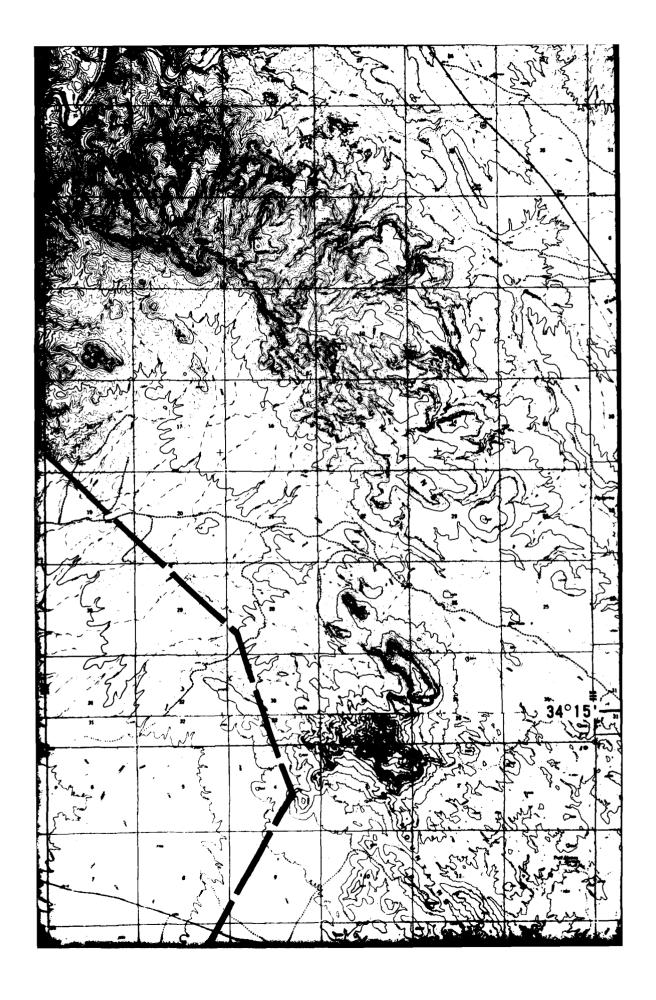
10 AUS 79

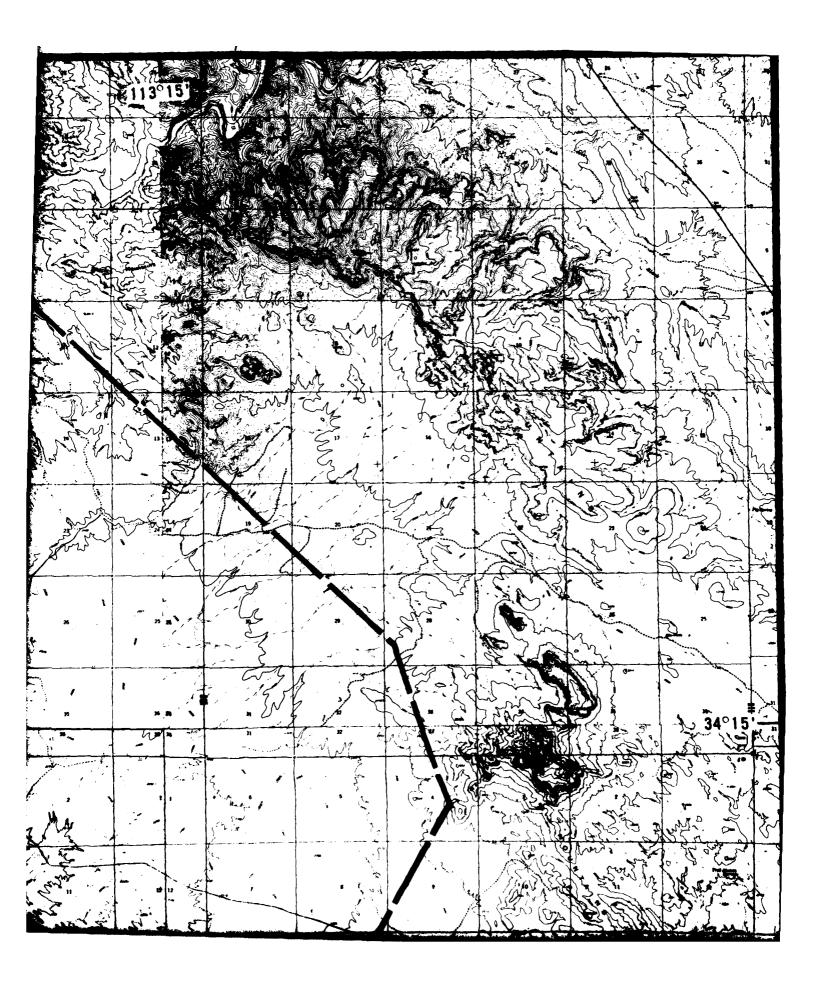


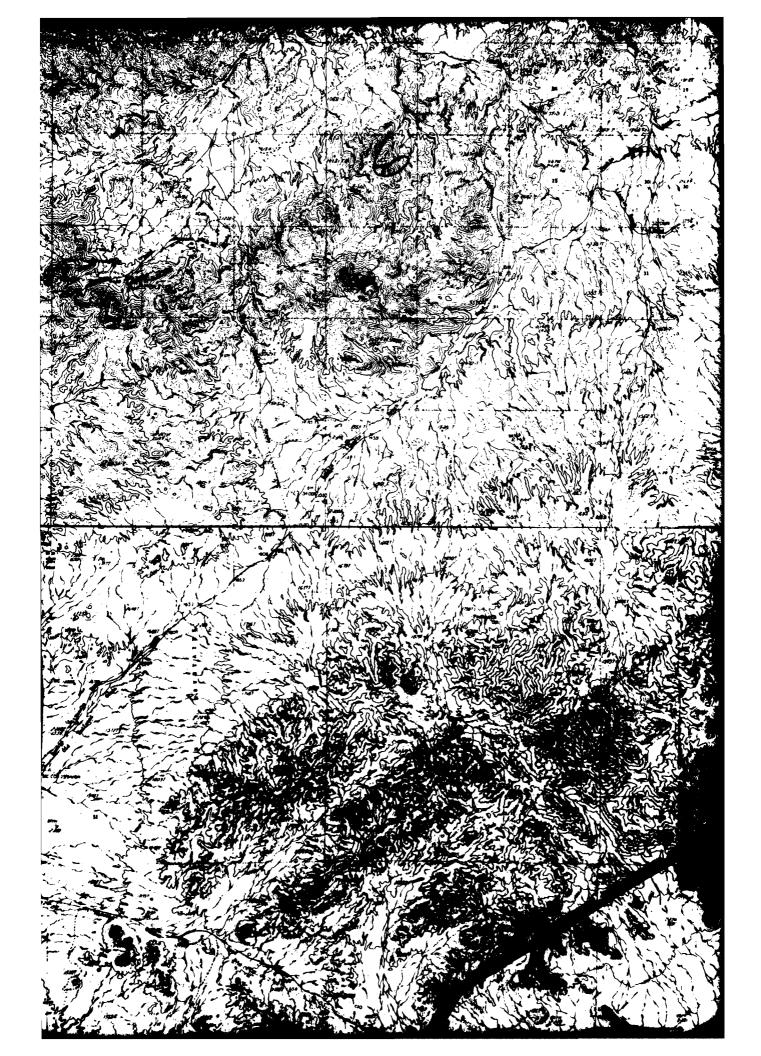




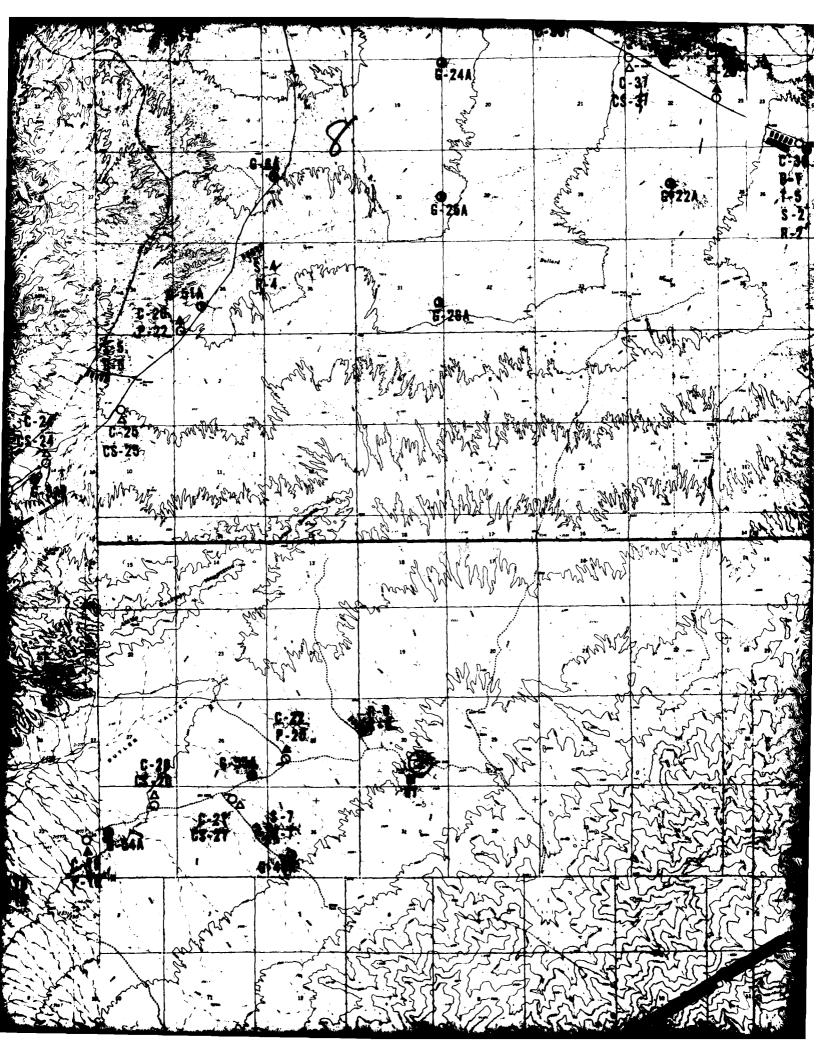


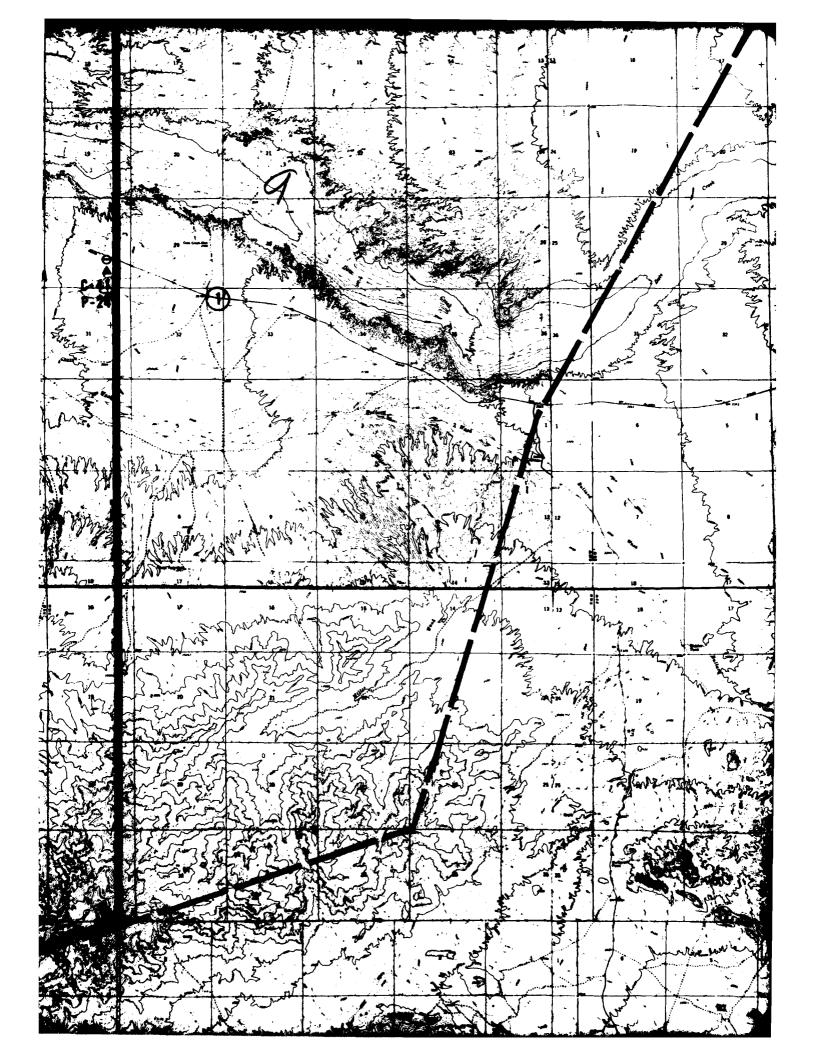


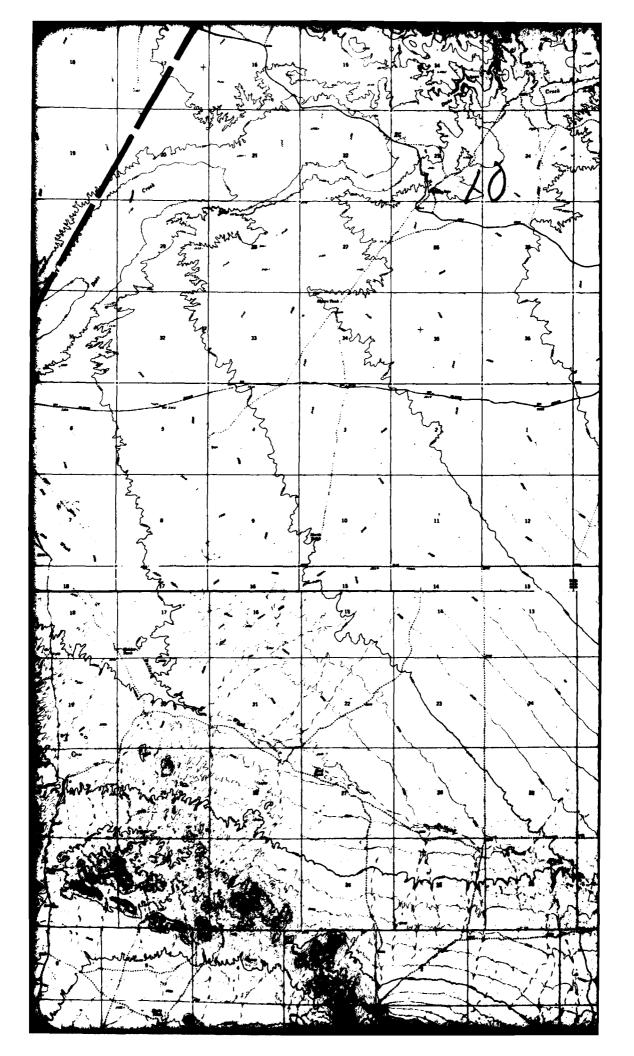


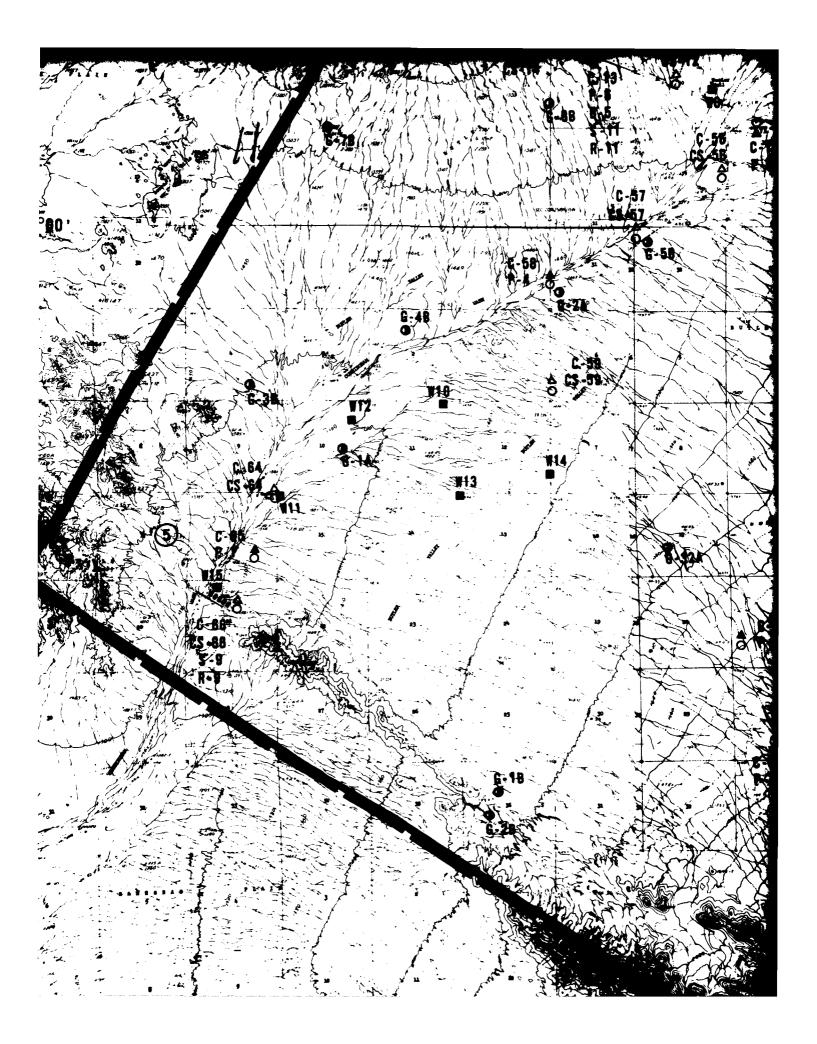


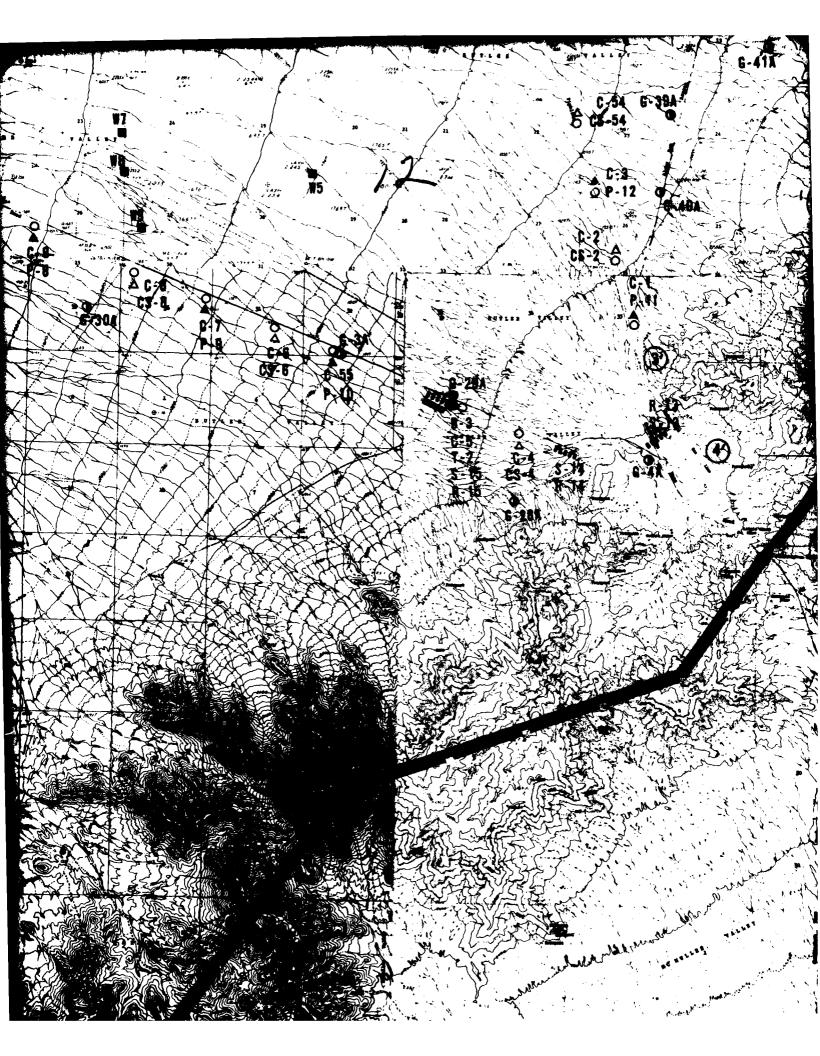


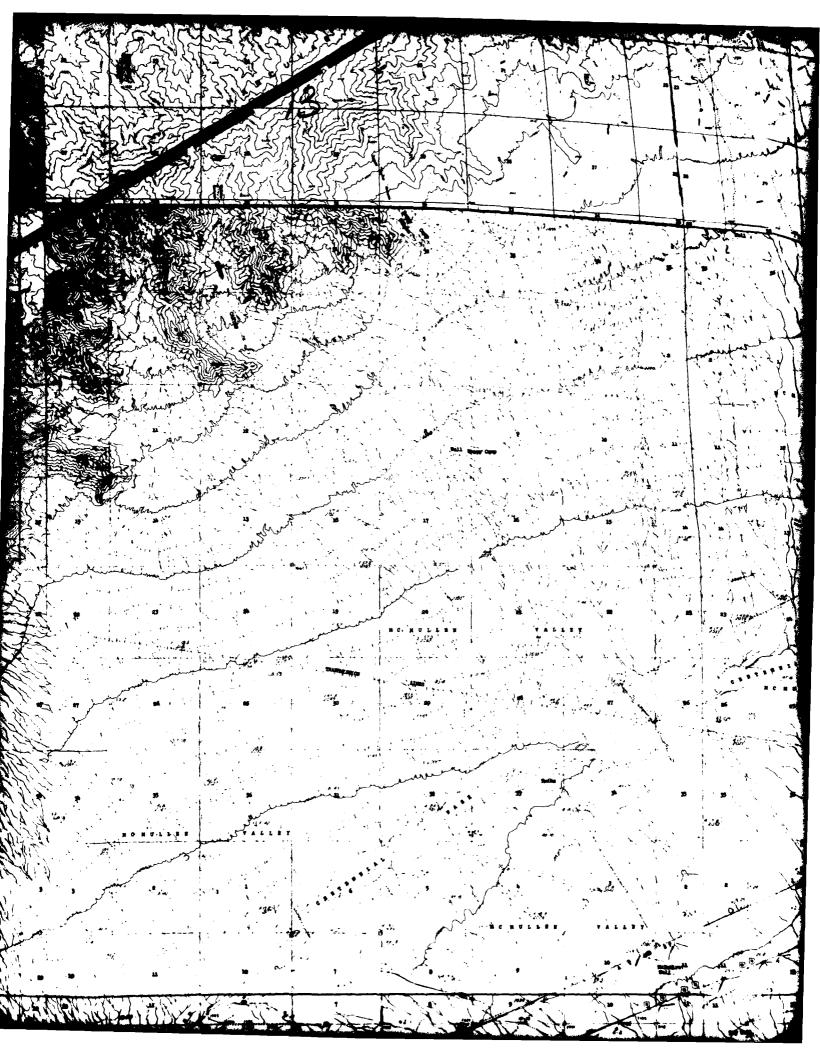


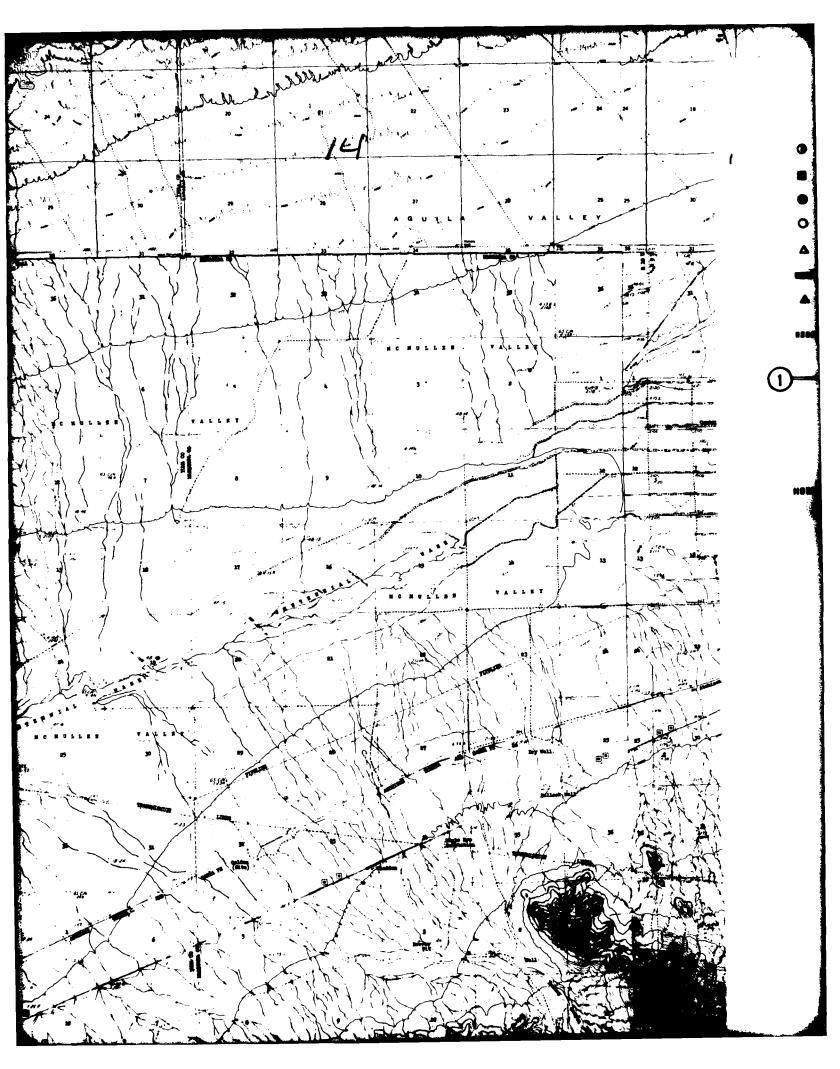




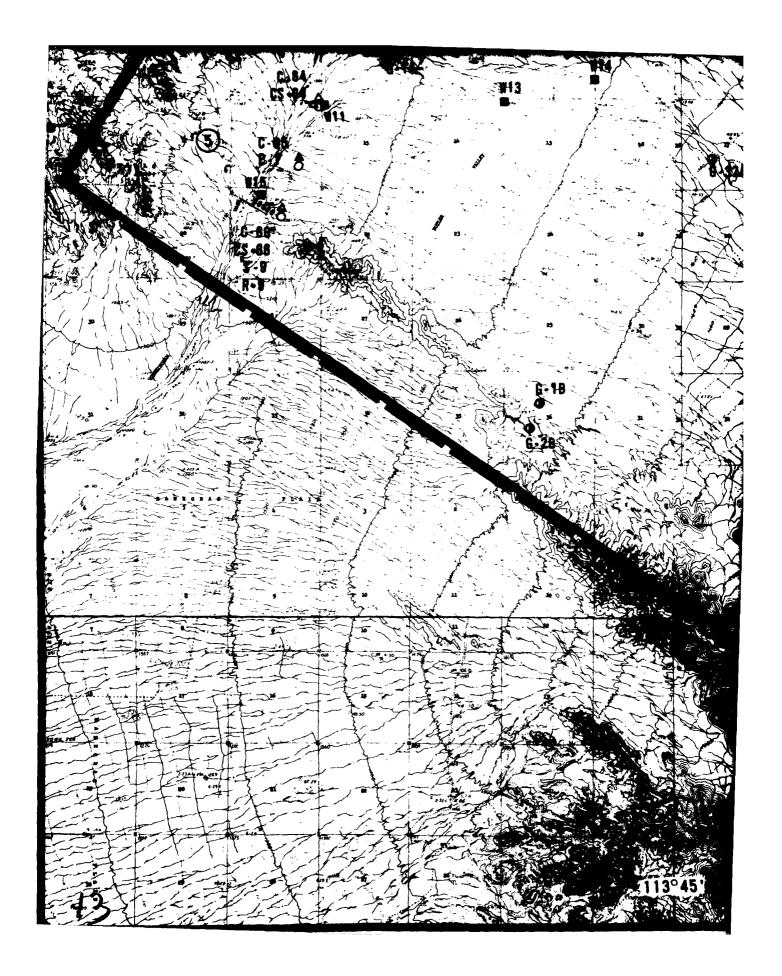


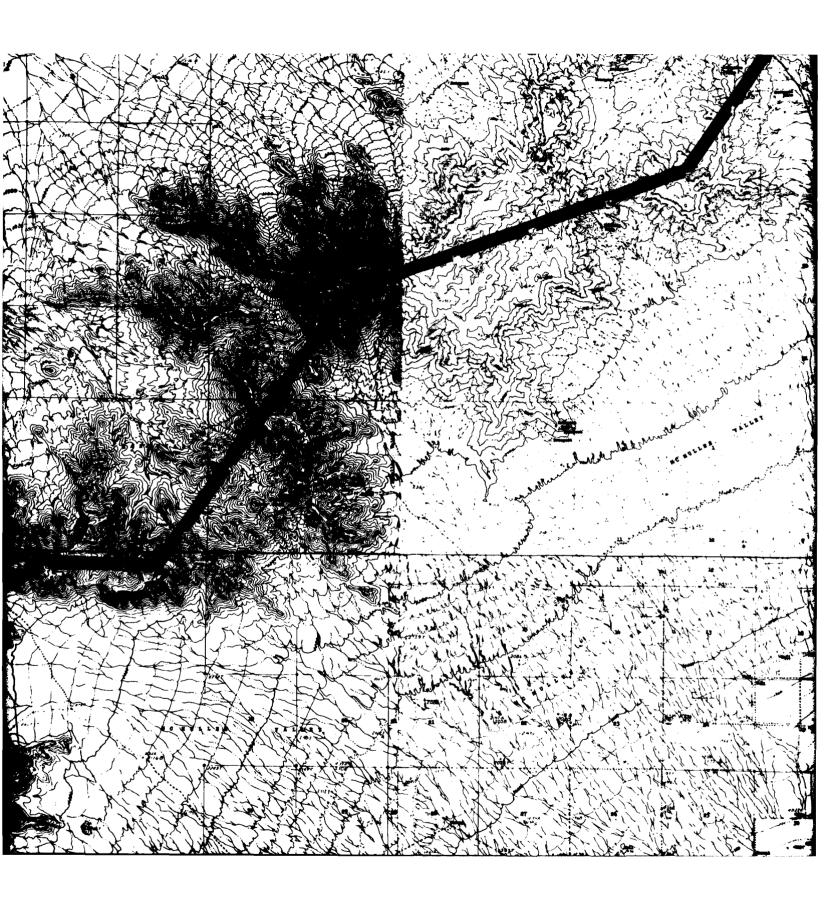


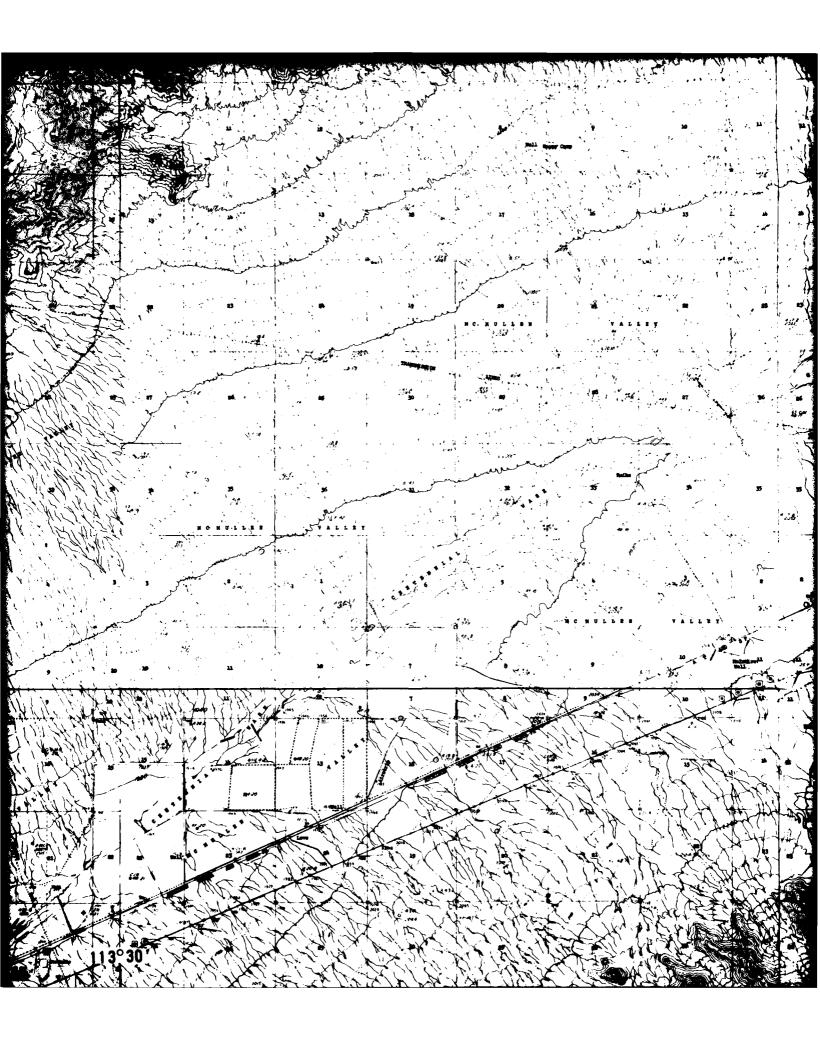


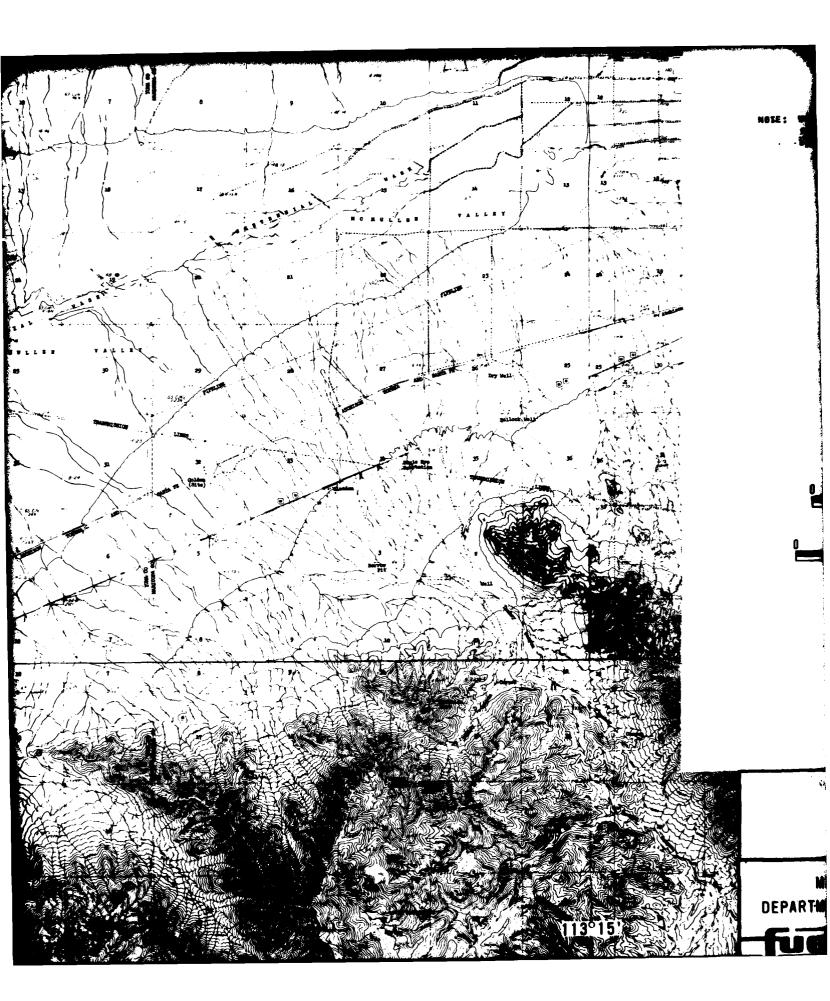


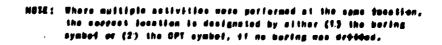
## EXPLANATION G-BA GEOLOGIC STATION GROUND-WATER LEVEL MEASUREMENT 8-1 BORFNG C-I COME PENETROMETER TEST (CPF) 34°00'-CS-1 SURFACE SAMPLE AT CPT LOCATION T-1 TRENCH P-1 JEST PIT S-1 SETSING REFRACTION LINE R-1 ELECTRICAL RESISTIVITY LINE ACTIVITY LINE NOTE: Where multiple activities were performed at the same tocation. the correct location is designated by either (1) the boring . - symbol or (2) the CPT symbol, if no besting was defilled. LOCATION MAP ARIZONA SCALE 1:82,500 NAUTICAL MILES 5,000 10,000







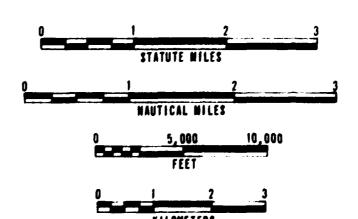




## LOCATION MAP



SCALE 1: 82,500



## ACTIVITY LOCATION MAP BUTLER CDP. ARIZONA

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

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1

UGRO NATIONAL INC.

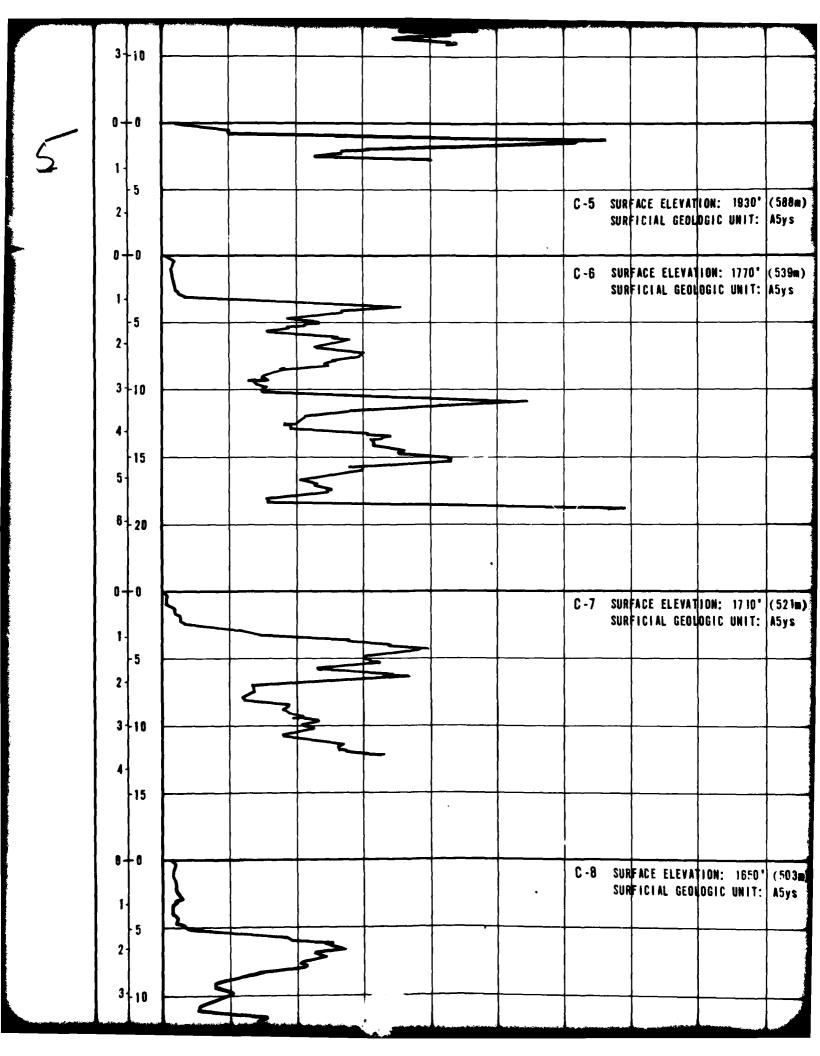
800	900 (kg/cn	n2)	DEPTH	100	200	300	400	500
0 800 800	900 (tsf)		O (FEET)	100	200	300	400	500
	300 (131)	SOIL COLUMN						<del></del>
		SP-SM	1 1 18				}	1
		(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	1 4 15					
		P-11	5		<b>~</b>	<del></del>		
CE ELEVATION: CIAL GEOLOGIC U	2030' (619m) NIT: Asis	<b> </b>	2-	7				}
,,,,,		1 1	3					
			3-10		<b>E</b>			
		CS -2	4-					
			15		<b>&gt;</b>			
	1		5-		$\Rightarrow$			
		} {	1 1 1		4	<del></del>	<del></del>	
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}		1 1						
E ELEVATION: 1	330° (588m)		0+0					
IAL GEOLOGIC U		M2				-		
		sc sc	5		-			
	}	P-12	2	<i>j</i>				Ì
	} }			}	<b>≥</b>		1	{
			3+10		<b>\</b>			
1	l l				>			}
	<b>!</b>		14					<b>-</b>
E ELEVATION - 2	040' (622m)		15					
R ELEVATION: 2 Hal geologic u	MIT: A5is	SP-SM	5 -					
-	1	CS -4						
			0+0	<b>=</b> 5				}
					=			
		}	1 1 1					
			5					
	1 1		111			}	}	Ì

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600	700	800	900 (kg/cm	<sup>2</sup> )	DEPTH
600	700	800	900 (tsf)	COLUMN	100 200 300 100 200 300
C-12	SURFACE EL SURFICIAL	EVATION: 153 Geologic Uni	00° (466m) T: A5ys	CS -12	
					0-0
					3-10
C-13	SURFACE EL SURFICIAL	EVATION: 150 GEOLOGIC UN	60° (475m) 1T: A5is	SC SM	0 + 0
					3 10
C-14					0-0
C-14	SURFACE EL	EVATION: 180 GEOLOGIC UNI	10° (488m) T: A5ys	CS -14	3-10

## CONE RESISTANCE

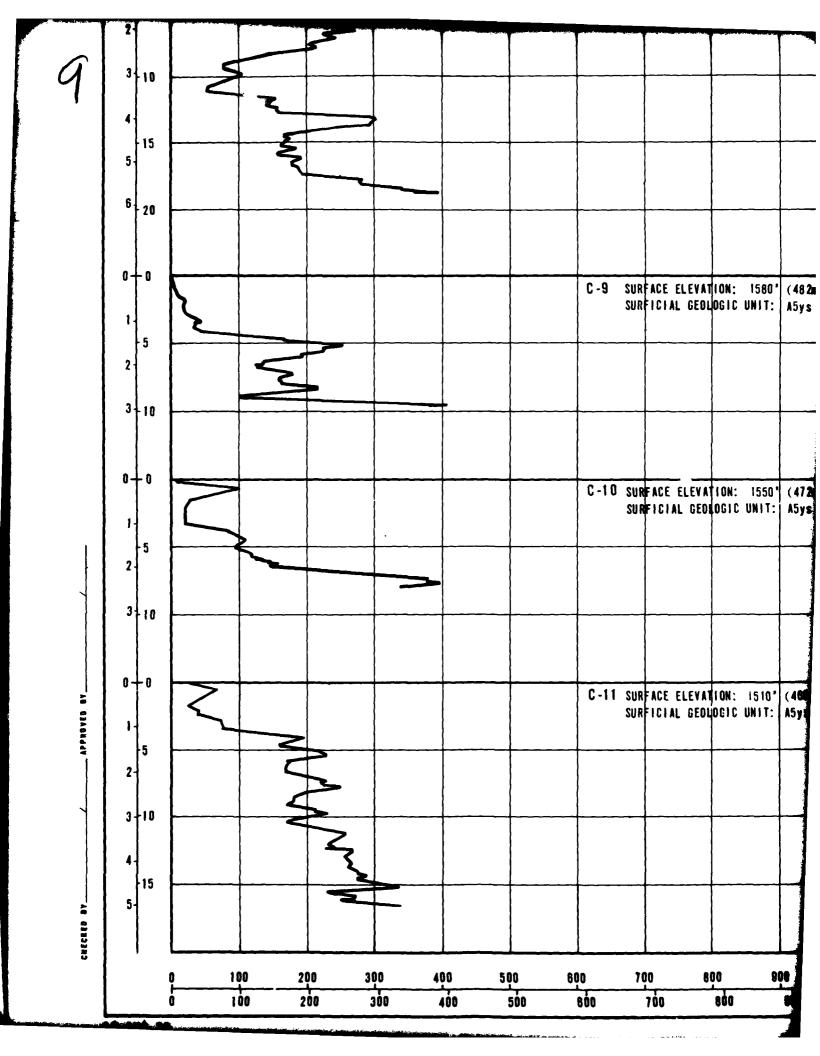
00 00	300	400	500	600	700	800	900 (kg/ci	
0	300	400	500	600	7Ò0	800	900 (tsf)	SOFL Column
		_		C -23	SURFACE E	LEVATION:	2020 (616m)	M2
_					SURFICIAL	GEOUOGIC U	NIT: A5og	GP-SM
_		==						P-21
				C -24	SURFACE E	LEVATION: 15	950' (594m) NIT: A5y A1s	SW-SM
	-				SURFICIAL	32000370 0	MII. POJ AIS	CS -24
-	2				1			
_								
				C -25	SURFACE E	LEVATION:	1910' (582m)	GP-GM
					SURFICIAL	. GEOL <mark>D</mark> GIC L	JNIT: A5ys	CS -25
=						-		
				-	•			
L								
							.	
r				C -26	SURFACE E	LEVATION:	1810' (552m)	GP-GM
	<b>-</b>				SURFICIAL	. GEOLOGIC I	UNIT: A5y.'A1s	
1								P-22
								<b>i</b> i i
		`						1   1
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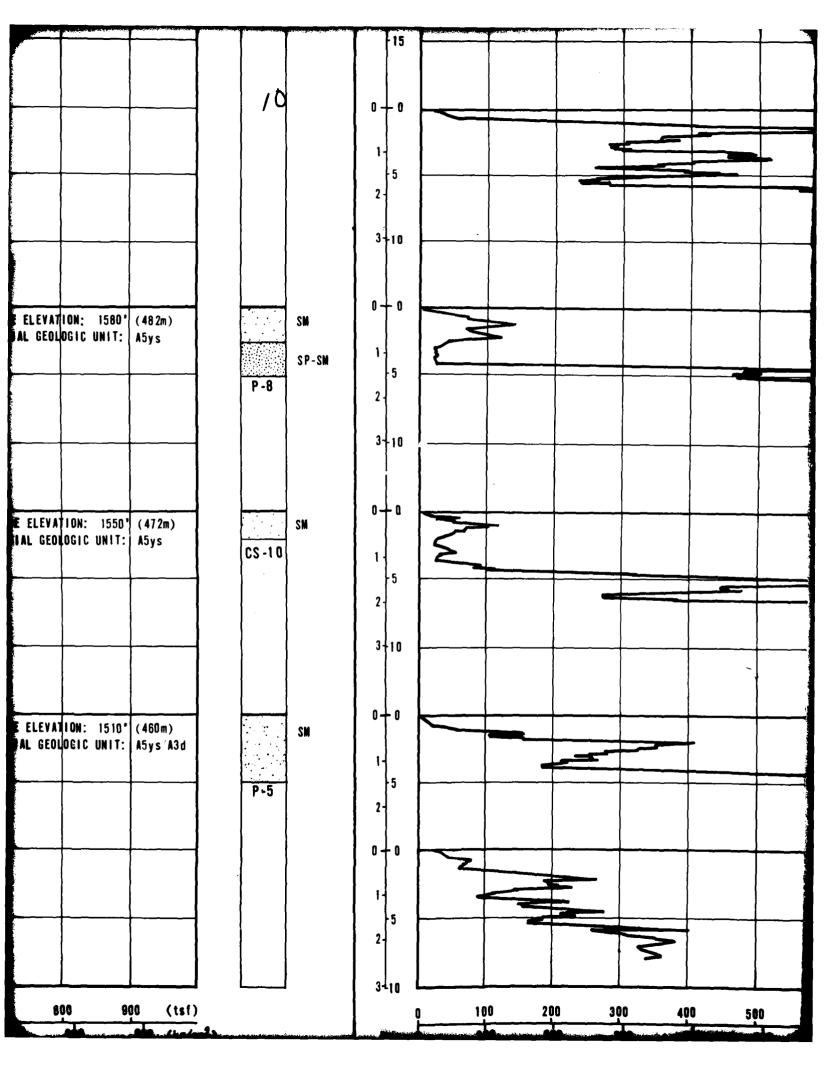


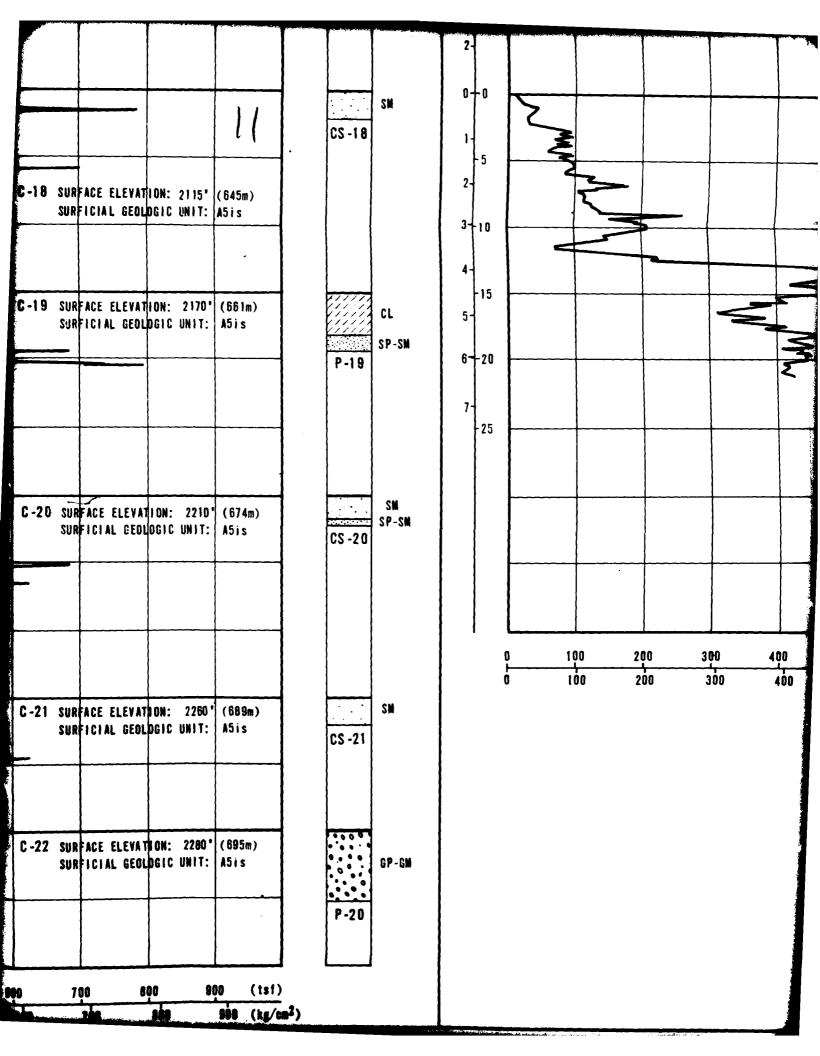
3	SURFICIAL GEOL	ION: 1930' (588 OGIC UNIT: A5ys ION: 1770' (539r OGIC UNIT: A5ys	n)	T-2 SM CS-6	2- 3-10 0-0 3-10 4- 15 5-	<b>\( \)</b>	
7 3	SURFACE ELEVA SURFICIAL GEO	ION: 1710' (521 DGIC UNIT: A5ys		ML P-9	3-10 4- 5- 5-		
8	SURFACE ELEVA Surficial Geo	TION: 1850' (503 Logic Unit: A5ys		CS -8	3-10 4- 15		

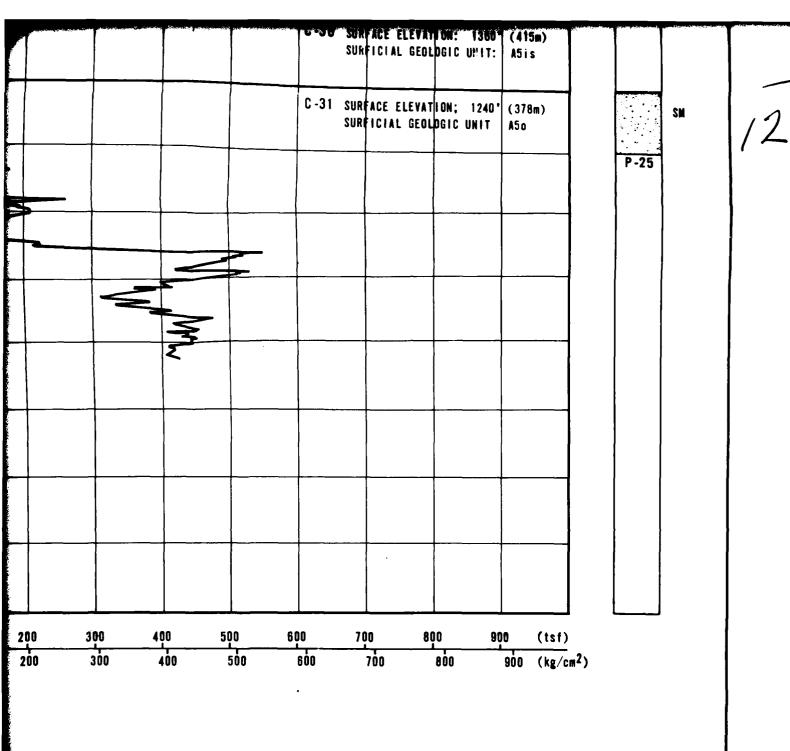
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SUR	ACE ELEVAT	ION: 1600° DGIC UNIT:	(488m) A5ys	CS -14	cı 7	2- 310		4 //		
SUR	FACE ELEVAT	ION: 1680° DGIC UNIT:	(512m) A5ig		SC SP-SC	0+0 1- -5 2-	2			
				P-7		0 + 0 1 - 5 2 - 3 - 10				
SUR	FACE ELEVAT	ION: 1985' OGIC UNIT:	(605m) A5ys	CS -16	SM	0-15 5- 0-0 1- -5 2-	20			
SUR	FACE ELEVAT	ION: 2045' DGIC UNIT:	(623m) A5is	P-18	SM GP-GM	3-10 4- 15 5- 6-20	•			
				F-10		0 <b>-0</b>				

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					-				CS -2	7	
				0.07						[	
						FACE ELEVAT Ficial geol	ION: 1500'	(457m) A5og			
		ı			3011	IDIAL GLOE	BOYO GRITT.	HOUE		ļ	
				C -28	CHD	TAPE ELEUAT	10N: 1425'	(424-)	27.77	র	
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	:			C -29	SUR	FACE ELEVAT	ION: 1350' DGIC UNIT:	(411m) A5is		SM	
					30 K	ICIAL GEOL	paic onii.	MU12			1
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				C-3N	SHR	ACE FLEVAT	ION: 1360'	(415m)			
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CONE PENETROMETER TEST RESULTS VERIFICATION SITE BUTLER COP. ARIZONA

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

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UGRO NATIONAL, INC.

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	CONE RESISTAN
<b>8</b> 00 900 (kg/cm²)	l de la companya de la companya de la companya de la companya de la companya de la companya de la companya de
800 900 (tsf) SOIL COLUMN	© 100 200 300 400 500 100 200 300 400 500
	O     S     S
GE ELEVATION: 1485 (453m) BIAL GEOLOGIC UNIT: A5ys	
	5
	2
	3-10
	4-
E ELEVATION: 1550 (472m)	15
FAL GEOLOGIC UNIT: A5ys	
	5
	2-
	3-10
	4
ELEVATION: 1820 ' (434m)	15
AL GEORGEIC UNIT ASYS	
	0+0
	1 2
·	2 5
	3-10
ELEVATION, 1900 (ELE.)	15
ELEVATION: 1890 (515m)	

The second secon

808	700	800	900 (kg/cm <sup>2</sup> )		DEPTH	400	•••	
600	700	800	900 (tsf)	SOIL	(FEET)	100	200	300 <b>400</b>
·	2 SURFACE EL SURFICIAL	EVATION: 142 GEOLOGIC UNI	25' (434m)	SP-SM SW-SM	3-10 (FEET) 2-15 5-15 5-15 5-15 5-15 5-15 5-15 5-15			
C -4	3 SURFACE EL SURFICIAL	EVATION: 19 GEOLOGIC UNI	045 (593m) T: A5ys	CS -43	7-25	7		
C-4	4 SURFACE EL SURFICIAL	EVATION: 18 GEOLOGIC UNI	95 (578m) 7: A5ys	CL SP-SM P-17	3+10			

CONE	RESISTANCE
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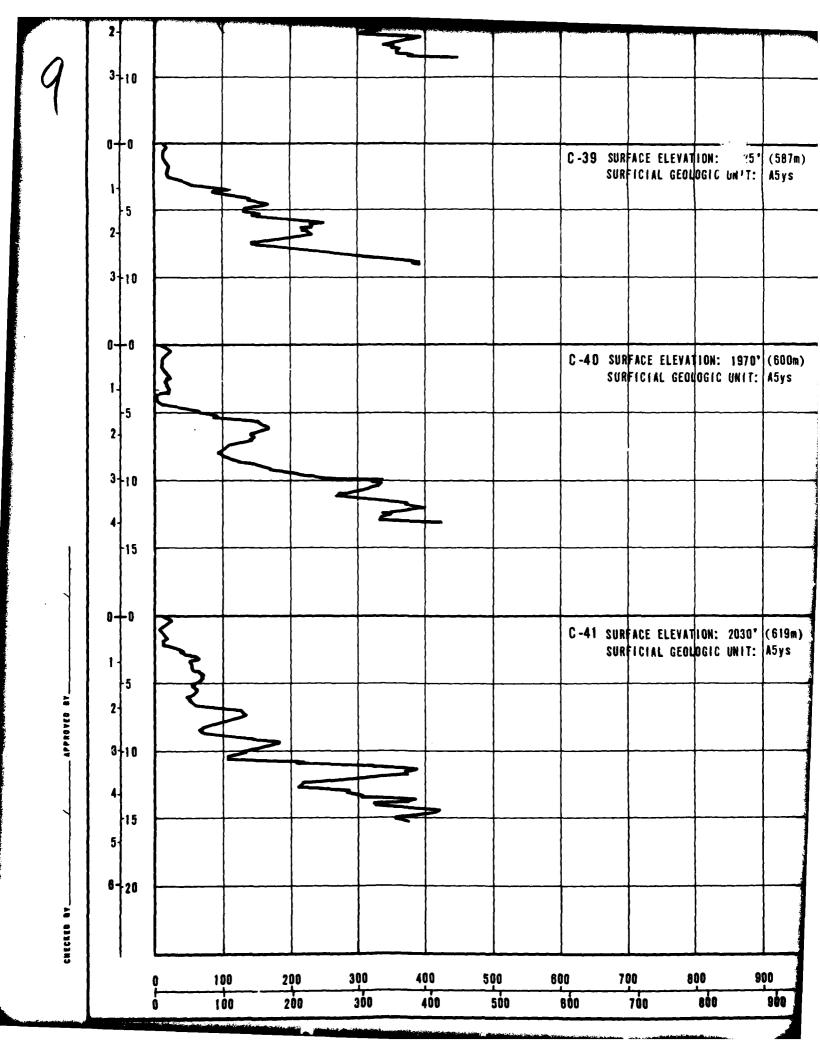
00 0	300	400	500	600	700	800	<b>8</b> 00	(kg/cm²)		
a	300	400	500	600	700	800	900	(tsf)	SOIL Column	
				C -52	SURFACE E SURFICIAL	LEVATION: GEOLOGIC (		55m) ys	CS -52	SM
	_									
-				C -53	SURFACE E SURFICIAL	LEVATION: GEOLOGIC	1840 (5 UNIT: A5	61m) ys		ML SC
									P-13	
				C -54	SURFACE E SURFICIAL	LEVATION: Geologic u	1880 (5 INIT: A5	73m) ys	CS -54	SM
						}	ł	4		

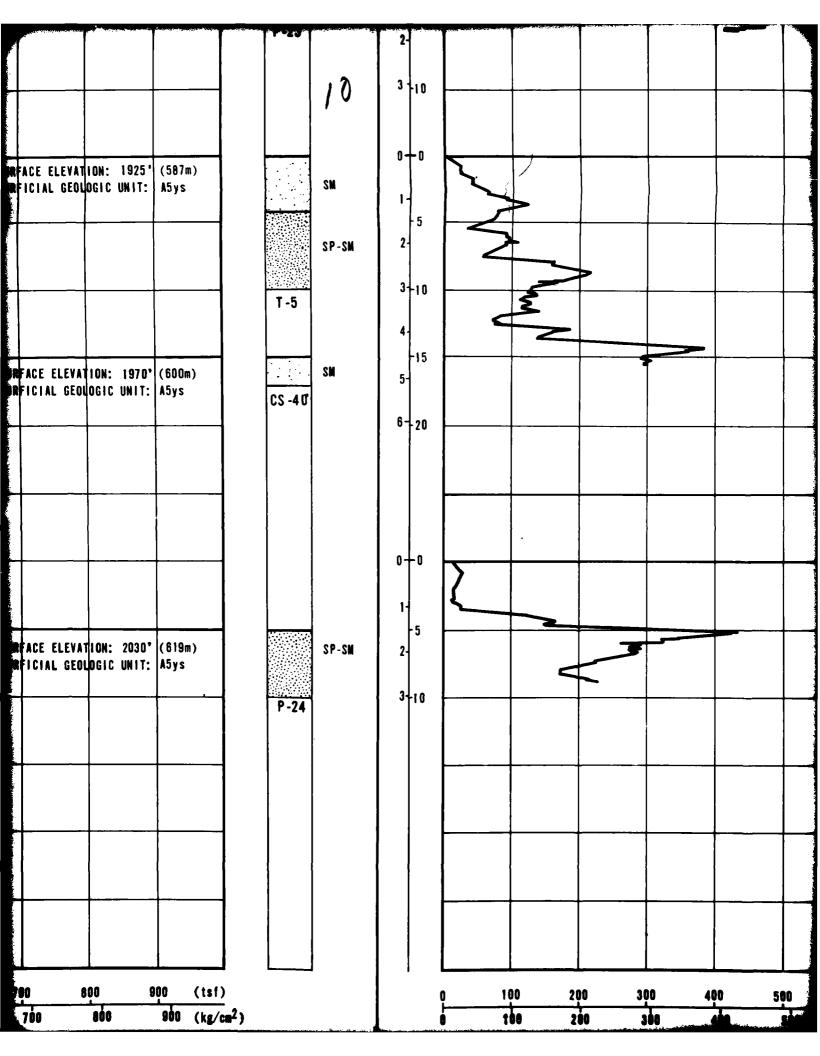
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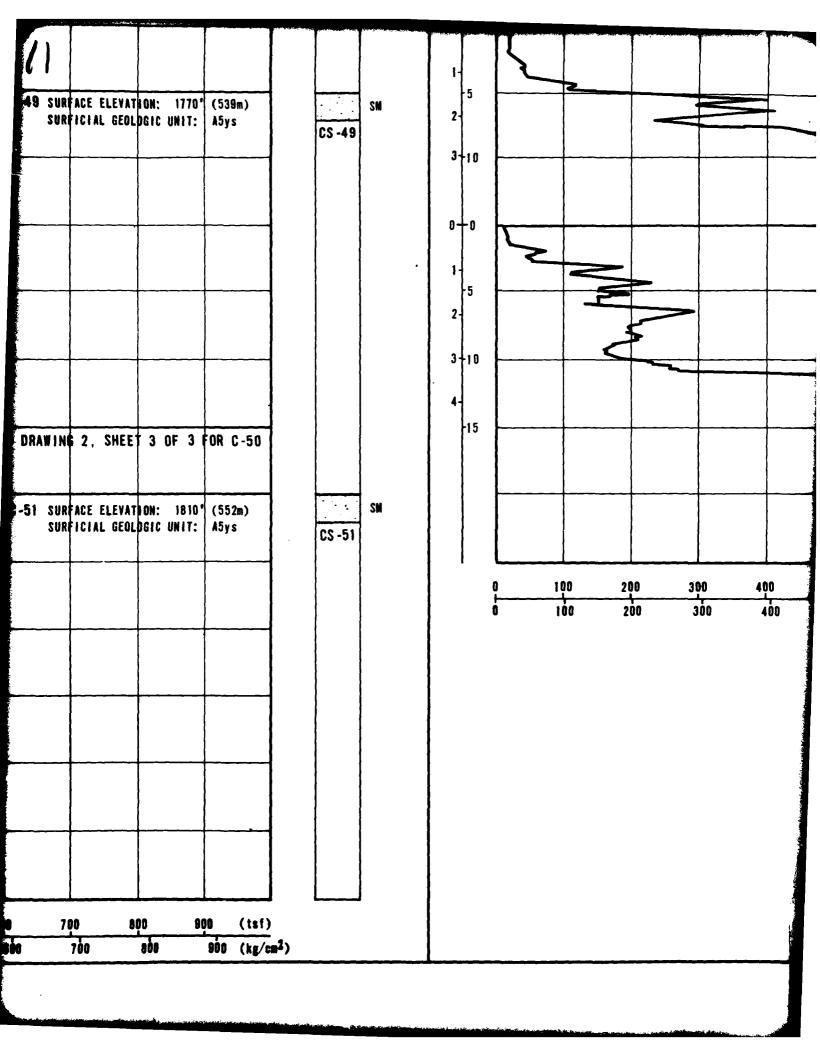
			1 5	
ELEVATION: 1750 ° AL GEOLDGIC UNIT:	(533m) A5ys	6	3-10	
			2-5	
E ELEVATION: 1810	(552m)	SM	3-10	
IAL GEOLOGIC UNIT:	A5ys	CS -37		
			3-10	
E ELEVATION: 1870'	(570m) A5ys	SM SP-SM P-23	1-5 2-1	
			3 10	
CE ELEVATION: 1925' CIAL GEOLOGIC UNIT:	(587m) A5ys	SM		
		SP-SM	2 2	

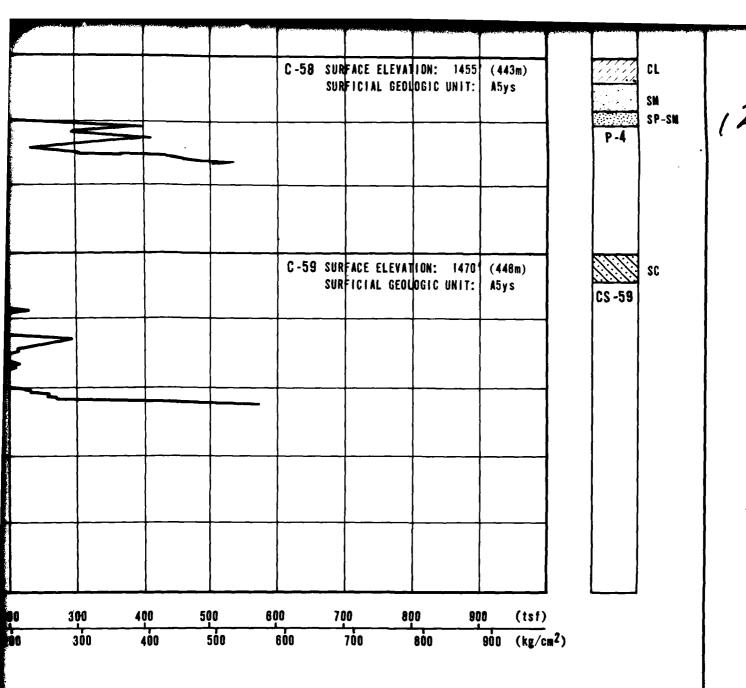
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					}				1				
								4-	ĺ				ļ
	C-46 SUR	FACE ELEVAT	ION: 1785°	(538m)	1	12		-11	5			<del></del>	
	SUR	FICIAL GEOL	DGIC UNIT:	A5ys	}	20 40	ML		I				
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CONE PENETROMETER TEST RESULTS VERIFICATION SITE BUTLER CDP . ARIZONA

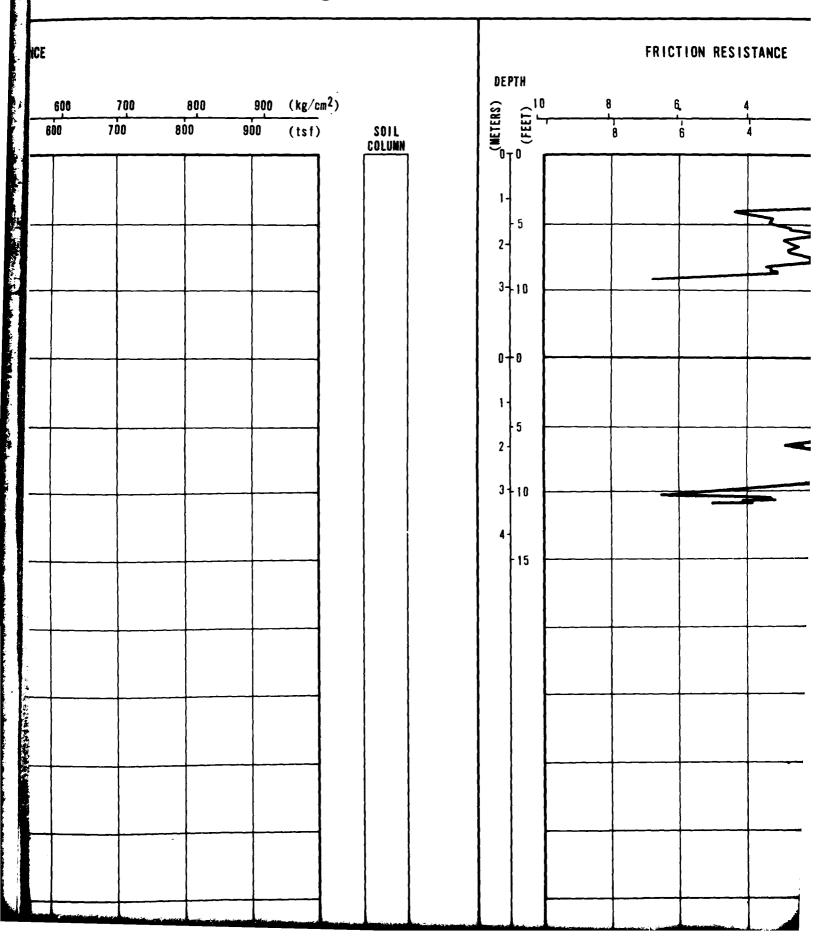
MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

DRAWING 2 OF 3

UBRO NATIONAL, INC.

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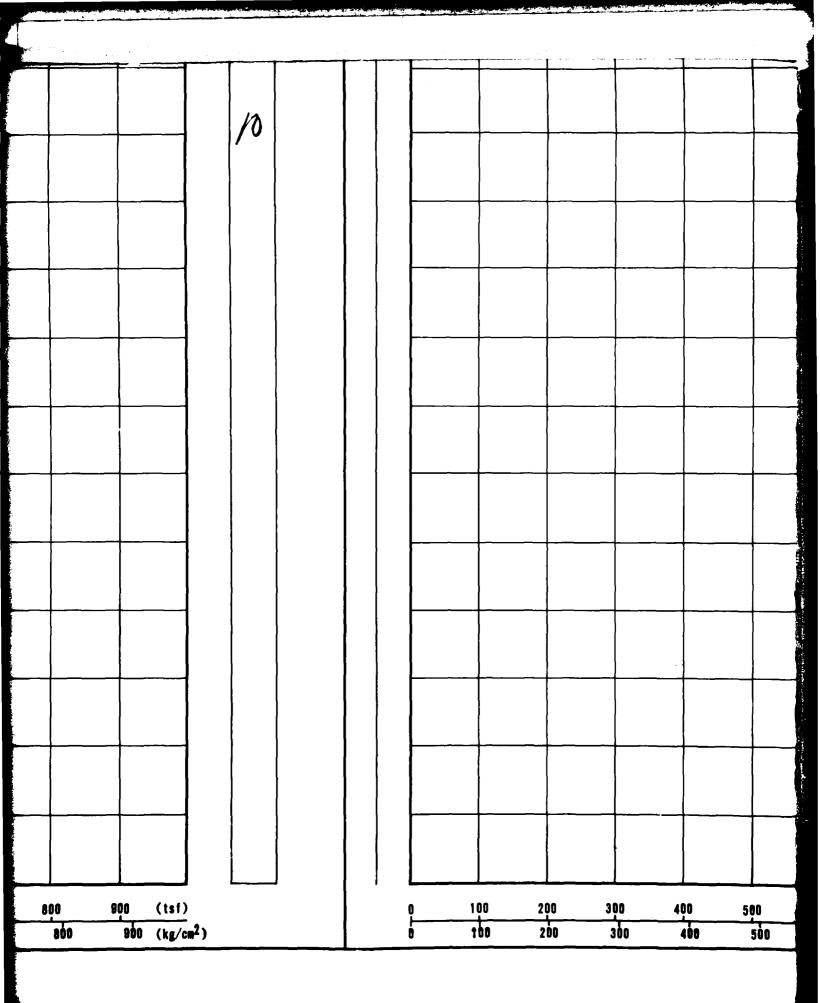
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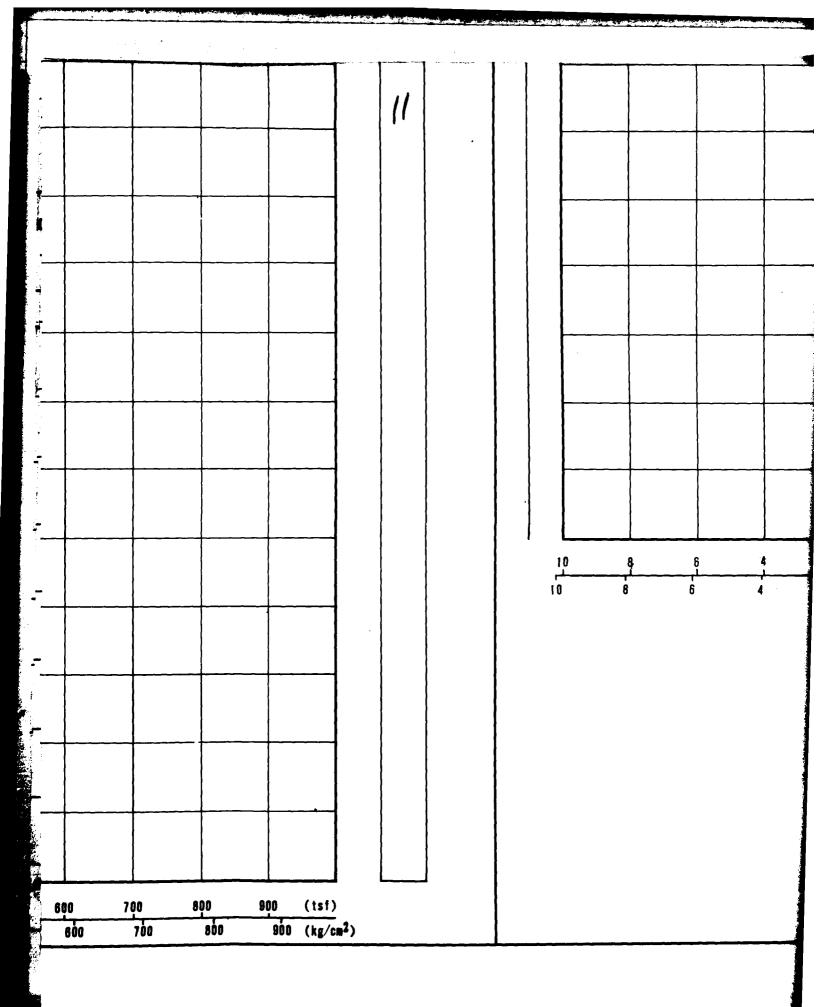
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